

TOWN OF MAMARONECK - VILLAGE OF LARCHMONT COASTAL ZONE MANAGEMENT COMMISSION Monday, April 22, 2019 7:30pm Mamaroneck Town Center, 1st Floor - Conference Room D, 740 W. Boston Post Road, Mamaroneck, NY 10543

Approval of Minutes

1. Approval of Minutes - March 25, 2019

Agenda Items

1. 7 Bay Avenue

Old Business

New Business

Meeting Adjournment

Any physically handicapped person needing special assistance in order to attend the meeting should call the Town Administrator's office at 381-7810.



Town of Mamaroneck — Village of Larchmont

COASTAL ZONE MANAGEMENT COMMISSION

TOWN CENTER: 740 West Boston Post Road, Mamaroneck, NY 10543-3353TEL: 914-381-7845FAX: 914-381-8473conservationdept@townofmamaroneck.org

CZMC Minutes - Draft March 25, 2019

A meeting of the Coastal Zone Management Commission (CZMC) was held on Monday, March 25, 2019 in the Mamaroneck Town Center, Conference Room D, 1st Floor, 740 W. Boston Post Road, Mamaroneck, New York. The meeting was called to order at 7:30 p.m.

MEMBERS PRESENT:

C. Alan Mason, Chairman Kanan Sheth Matthew Teitsch Robert Fletcher Maurizio Bertini

OTHERS PRESENT:

Councilwoman Jaine Elkind Eney, Liaison to Town of Mamaroneck Town Board Elizabeth Paul, Environmental Planner, Town of Mamaroneck Josh Lawlor, Applicant, 1 Briarcliff Road Ralph Alfonzetti, Engineer, 1 Briarcliff Road Michael Piccirillo, Architect, 1 Briarcliff Road Azure Dee Sleicher, P.E. Race Coastal Engineering, 14 Pryer Lane Benedict Salanitro, Engineer, Bonnie Briar Country Club

1. Approval of Minutes

The minutes of the February 25, 2019 meeting were approved as submitted.

2. **Referral – 1 Briarcliff Road**

CZMC visited the property at 1 Briarcliff Road on March 11th. Architect, Vladimir Levin and Engineer, Ralph Alfonzetti were at the site visit answering questions. At tonight's meeting, Architect Michael Piccirillo and Engineer, Ralph Alfonzetti continued the presentation and discussion of the proposal. CZMC members expressed concerns about the ability of the proposed house and stormwater system to withstand a catastrophic flood event. The engineer stated that to protect the house, the foundation can be reinforced and will have flood vents installed. In addition, the mechanicals can be suspended from the ceiling or placed in the attic. The stormwater system and raingarden have been sized to handle a 25-year storm, which is what it is required to do. The homeowner is aware that the property floods and appears prepared to accept this risk.

CZMC found the proposal to be consistent with the policies in the LWRP. As designed, the proposal includes the minimum measures required for stormwater mitigation.

However, it is recommended that additional reinforcement be provided for the foundation, and additional precautions be taken to make the property as resilient to the impacts of future flooding as possible.

3. **Referral – 14 Pryer Lane**

Azure Dee Sleicher, from Race Coastal Engineering presented the proposal to repair the seawall and install a gangway and floating dock at 14 Pryer Lane. The ramp as proposed will be 25-feet long leading to a 12×16 foot floating dock to be located in the Premium Mill Pond. The applicant is seeking approvals from the Army Corps of Engineers, NYS DEC and the NYS Office of General Services and was referred by the NYS Department of State for local consistency review.

CZMC found the proposal to be consistent with the policies in the LWRP with the restriction that no lighting shall be permitted on the ramp or dock and use of the dock should be limited to non-gas powered boats. In addition, the applicant must acquire the required underwater land grant, easement or lease necessary prior to installation.

4. **Referral – Bonnie Briar Country Club**

Benedict Salanitro presented the proposal for the replacement of 8 bridges and various watercourse landscape and maintenance activities throughout the golf course requiring a Wetlands and Watercourses Permit from the Town of Mamaroneck Planning Board. Watercourse maintenance includes the removal of accumulated leaves and sediments from the Sheldrake River, water features and irrigation ponds, the removal of invasive plants and the repair of eroded river banks. The bridges are primarily pedestrian and golf cart bridges and will be replaced with prefabricated bridges that will have landings beyond the banks of the river. Work will be divided into manageable phases over the course of several years requiring one or more permit extensions.

CZMC found the proposal to be consistent with the policies in the LWRP provided that the all required permits for the proposed maintenance activities are obtained, best management practices are followed for erosion and sediment control and restoration of disturbed areas occurs promptly. If the Planning Board determines that they would like CZMC to provide additional review of any of the project elements in the future, this can always be done.

5. **Referral – Issuance of NY Transportation Regional General Permit (TRGP-1)**

CZMC reviewed the draft New York Transportation Regional General Permit (TRGP-1) for certain transportation related activities in New York State. The New York State Department of State referred it to communities with local LWRPs for a consistency review.

The current permit would be revised to allow the following activities:

- Maintenance Activities
- Linear Transportation Projects
- Non-Linear Transportation Projects
- Streambed and Bank Stabilization Activities

- Temporary Construction, Access, Dewatering
- Emergency Activities

Under the proposed permit, non-tidal wetlands of up to 2 acres in size can be filled (the existing permit limits the filling of wetlands to 1/2 acre) and up to 500 linear feet of stream bed can be lost (previously, only the amount necessary could be lost).

CZMC found the proposed changes to the permit to be inconsistent with the policies in our Local Waterfront Revitalization Program. Specifically, Policy 44 which states, "Preserve and Protect Tidal and Freshwater Wetlands and Preserve the Benefits derived from these areas." Locally, freshwater wetlands as small as 2500 square feet and all watercourses are protected. These smaller wetland areas and vernal pools provide significant local wildlife habitat, flood mitigation and water quality benefits and should be preserved.

The draft permit frequently uses the term, "maximum extent practicable" as a standard for protection of habitat, wetland areas and watercourses. This term is vague and vulnerable to misinterpretation. Standards for protection must be clearly defined in order to make them enforceable.

The permit should not be modified to include new linear transportation structures or new non-linear transportation structures. These are not time-sensitive projects and should go through normal review procedures. Changes to the existing permit should be limited to in-kind and in-place repairs or replacements of structures and emergency activities. The draft permit should clarify that any transportation projects occurring within the Town of Mamaroneck or Village of Larchmont must be referred to our local Coastal Zone Management Commission for consistency review and any local permits.

6. **Old Business**

No old business to discuss.

7. New Business

The New York State Board for Historic Preservation is considering Winged Foot Golf Club for inclusion on the National and State Registers of Historic Places. This will require any unlisted action occurring within or adjacent to the property to be considered a Type I action under SEQR. Because the property is a Critical Environmental Area, this was already the case.

The meeting was adjourned at 9:00 p.m.

Town of Mamaroneck - Village of Larchmont Coastal Assessment Form (CAF)

Applicants, or the appropriate municipal agency, shall complete this Coastal Assessment Form (CAF) for proposed actions which are subject to Local Consistency Review (see Waterfront Revitalization Law §§234-1 through 234-5 in the Code of the Town of Mamaroneck and §§292-1 through 292-4 in the Code of the Village of Larchmont). This assessment is intended to supplement other information used by the Bi-Municipal Coastal Zone Management Commission in making a determination of consistency with the Town of Mamaroneck and Village of Larchmont Local Waterfront Revitalization Program.

Upon completion of this form, it should be submitted as part of a complete application package for review. If assistance or further information is required for Town of Mamaroneck matters, please contact the Town of Mamaroneck Environmental Planner at (914) 381-7845. For Village of Larchmont matters, please contact the Village of Larchmont Building Inspector at (914) 834-6210.

PLEASE PRINT OR TYPE ALL ANSWERS.

A. GENERAL INFORMATION

Will the proposed action be undertaken by a municipal agence	cy? Y	les []	No [🗡]
If yes, please list agency or agencies and contact person(s): _				

If no, please complete the applicant information:						
Name of	Name of Applicant: Stephen Wang & Associates PLLC					
Street Ad	ldress:	950 Third	Avenue, 4th Fl	loor		
City, Stat	te, Zip:	New York,	NY 10022			
Phone: _	212.829.9494	Fax:	N/A	Email:	stephen@swarchitect.com	

Location and ownership of property for which action is proposed:

Section:	Block:30	Lot: 729
Owner of Property:	Mr. & Mrs. Segal	
Street Address:	7 Bay Avenue	
City, State, Zip:	Larchmont, NY 10538	
Phone: 212.829.9494	Fax:N/A	Email:stephen@swarchitect.com

Size of property (square feet): _	40,549 S.F.	Is the property now developed?	Yes [🗙]	No []
Will project require a zoning van	riance? Yes [] No	⊳ ⊳4			
If yes, briefly describe:					

Describe any unique/unusual landforms on the project site (rock outcroppings, swales, etc.): The project site is located on the Long Island Sound, protected by a seawall. The seawall is interrupted by an outcropping of bedrock, while the front yard also has an outcropping of bedrock. The site slopes down to the Sound.

Percentage of site which contains slopes of 25% or greater: 0%

Are there streams, lakes, ponds or wetlands existing within or contiguous to the project area? If so, describe (name, size, characteristics): No.

Will the action require approval by a state or federal agency? Yes [] No [**×**] If yes, specify which state or federal agency and attach a copy of pending application and any relevant information and/or documentation to this form:

B. DESCRIPTION OF SITE AND PROPOSED ACTION

Provide a written description of the nature and the extent of the proposed action. Attach plans or additional information as necessary and/or required by application procedures.

Construction of a single family residence as of right, with previously approved pool and associated

storm-water management practice.

Architectural site plan, site survey, and Storm-water Management Plan and Drainage Analysis Report

are included with this application.

C. COASTAL ASSESSMENT

Check either "Yes" or "No" for each of the following questions:

1. Will the proposed action be located in, or contiguous to, or have a **potentially adverse effect** upon any of the following designated resource areas?

	Yes	No	Maybe
a.	Significant fish or wildlife habitat or designated critical environmental area[X]	۲.]	[]
b.	Scenic resources of local significance[]	$\left \times\right $	[]
c.	Natural protective features in an erosion hazard area[]	[>]	[]

NOTE: If the answer to any of the above questions is "Yes", please explain in Section D any measures which will be undertaken to mitigate the adverse effects.

2. Will the proposed action have a significant effect upon:

		Yes	No	Maybe
a.	Commercial or recreational use of fish and wildlife resources	[].	[X]	[]
b.	Scenic quality of the coastal environment	i i.		i i
c.	Development of future, or existing water dependent uses	[].	$[\mathbf{x}]$	[]
d.	Land or water uses within a small harbor area	ĹĴ.		[]
e.	Stability of the shoreline	Ĩ.	$[\times]$	Î Ì
f.	Surface or groundwater quality	ĺ Ì.		Î Î
g.	Existing or potential public recreation opportunities	Î Ì.	[Xi	Î Î
h.	Structures, sites or districts of historic, archeological or cultural significance			
	to the local area, state or nation	.[]	[X]	[]
3.	Will the proposed action involve or result in any of the following:			
	1 1	Yes	No	Maybe
a.	Physical alteration of land along the shoreline,			•
	land underwater or coastal waters	[]	$[\times]$	[]
b.	Expansion of existing public services or infrastructure in or near		•	
	undeveloped or low density areas of the coastal area?	[]	[X]	[]
c.	Filling, dredging, excavation or mining in coastal waters	[]	1×1	[]
d.	Reduction of existing or potential public access to or along the shore	[]	$[\times]$	[]
e.	Development within a designated flood or erosion hazard area	[]	$[\times]$	[]
f.	Development of a natural feature that protects against flooding or erosion	[×]	[/]	[]
g.	Replacement of eroded sand or soil	[]	×	[]
h.	Construction or reconstruction of erosion protective structures	[]	[×]	[]
i.	Any change in surface or groundwater quality	[]	[X]	[]
j.	Removal of trees from the site	[]	[X]	[]
4.	Project details:			
		Yes	No	Maybe
a.	If the project is to be located adjacent to the shore:			
	1. Does the project require a waterfront site in order to function	[]	[×]	[]
	2. Will water-related recreation be provided	[]	[X]	[]
	3. Will public access to shore or state owned underwater lands be provided	[]	$[\mathbf{X}]$	[]
	4. Will it replace a recreational or maritime use	[]		[]
	5. Do essential public services and facilities presently exist at or near the site	L I	[×([]
1110				

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	6. Is the site located near a flood prone area	[]]	[]
	7. Is the site located in an area of high erosion	$[\times]$	Ī	j
b.	Is the site presently used by the community as an open space or			-
	recreation area[]	$ \mathbf{X} $	[]
c.	Does the project site offer or include scenic views/vistas known to be			
	important to the community or the state	[×]]]
d.	Will the surface area of any waterways or wetland areas be increased or			
	decreased by the project	$[\times]$	[]
e.	Will the project involve any waste discharges into coastal waters	$[\times]$]]
f.	Does the project involve discharge of toxins, hazardous substances or other			
	pollutants into coastal waters	$[\boldsymbol{\times}]$	[]
g.	Will the project affect any area designated as a tidal or freshwater wetland[]	$[\times]$	[]
h.	Will the project result in an alteration of drainage flow patterns or surface			
	water runoff on or from the site	[]	[]
i.	Will best management practices (BMPs) be utilized to control			
	stormwater runoff	[]	[]
j.	Will any aspect of the proposed project result in emissions which exceed			
	federal or state air quality standards or generate significant amounts of			
	nitrates or sulfates[]	[×]	[]

Please explain any of the above answers that may need further clarification in Section D.

D. COMMENTS AND ADDITIONAL INFORMATION: (continue on back if necessary)

As designed, runoff from the proposed roof and previously approved pool and patio will be conveyed to a proposed rain garden for water quality treatment prior to conveyance to a proposed attenuation gallery which will control the runoff prior to entry into the sound. The proposed attenuation gallery will discharge into the Long

Island Sound through an overflow pipe where disturbance should not exceed 10 square feet.

H:\CZMC\ADMIN\CAF9-29-10.doc Page 4 of 6 D. COMMENTS AND ADDITIONAL INFORMATION: (continued)

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	_

I certify that I am the above described applicant and that the information contained on this form and on the attached survey/site plan(s) is(are) accurate to the best of my knowl¢dge.

Date: 04/09 2019 5 Signature of Applicant Prepared by: (if different than the applicant) Name and Title: Agency/Company: Street Address: City, State, Zip: -----Phone: _____Fax: ____Email:_____

I certify that I prepared this Coastal Assessment Form for the above described applicant and that the information contained on this form and on the attached survey/site plan(s) is(are) accurate to the best of my knowledge.

Date: ______ 20 _____

Signature of Preparer



			_	Stephen W	lang +	Associates PLLC
ANAL	YSIS	3/27/19		A R C	ні	TECTS
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				New York, NY 10 (212) 829 9494 t	022	
of Lot 1	1 and Part of Lot 2)			(212) 829 9409 f		
e-fami	ly Residence				© 20	18 Stephen Wang & Associates PLLC
			PI	ROJECT:		
	Per New Codes	Proposed		SINGL	E FAM	ILY RESIDENCE
F		40,549 SF		71	BAY AVEN	UE, LARCHMONT
	120 FT (Min)	155 FT			NEW YOR	K, NY 10538
Г	30 FT (Min)	± 35.3 FT				
Γ	50 FT (Min)	± 82.3 FT				
	26.94 FT	± 34.9 F1		CLIENT: PRIVATE RESIE	DENCE	
	59 88 FT	+ 72 FT		INTERIOR DES	IGNER:	
	14 192 15 SF	- / - / - /		CHANGO & CO 226 GRAND ST	REET, BROO	KLYN, NEW YORK 11211
7 SF	(Max - 35%)	13.441.46 SF		T: 718.487.9559 F: 347.696.7714	ł	
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'SIS				BLUE SKY DES 121 WEST 27TH	IGN, INC I STREET, SI	JITE 904, NY, NY 10001
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9	12,975.68 SF	12,973.45		MECHANICAL	ENGINEER:	
				OLA CONSULT 50 BROADWAY	NG ENGINEE , 2ND FL, HA	ERS, PC WTHORNE, NY 10532
				T: 914.747.2800		
IS				LANDSCAPE A JANICE PARKE	R LANDSCA	PE ARCHITECTS
	Remove/Add	Proposed		19 WEST PUTN T: 203.340.2824		, GREENWICH, CT 06830
SF	-18.91 SF	3,139.79 SF		CIVIL ENGINEE	R:	
SF	129.97 SF	5,094.48 SF		HUDSON ENGI 45 KNOLLWOO	NEERING & (D ROAD, #20	CONSULTING, P.C. 11, ELMSFORD, NY 10523
SF	1,556.30 SF	4,739.18 SF		T: 914.909.0420		
SF	-1,721.50 SF	0.00 SF		GENERAL CON MURPHY BROT	ITRACTOR: THERS CONT	RACTING, INC.
	N/A	Inclusive		416 WAVERLY / T: 914.777.5777	AVENUE, MAI	MARONECH, NY 10543
9 SF	-54.14 SF	12,973.45 SF				
				M	AX. TOTAL SC	QFT: 12,975.68 SQFT
mula (PER NEW ZOINING	CODES)				
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ASPHALT TOP -(FINISH COAT ASPHALT -BASE COAT COMPACTED — CRUSHED STONE UNDISTURBED -SOIL

8"

NOTE: EXPANSION JOINTS TO BE INSTALLED EVERY 10 FEET. CONCRETE CURB

CONCRETE WASHOUT AREA NOTES:

- 1. CONCRETE WASHOUT AREA TO BE INSTALLED PRIOR TO CONCRETE PLACEMENT ON
- CONCRETE WASHOUT AREA TO BE INSTALLED PRIOR TO CONCRETE PLACEMENT ON SITE. CONCRETE WASHOUT AREA TO BE ENTIRELY SELF CONTAINED
 HAY BALES SHALL BE PROVIDED AROUND THE PERIMETER OF CONCRETE WASHOUT AREA FOR CONTAINMENT.
 WASHOUT AREA SHALL BE LINED WITH PLASTIC SHEETING NO THINNER THAN 10 MILS. SHEETING SHALL HAVE NO HOLES OR TEARS AND SHALL BE ANCHORED BY SAND BAGS ON ALL SIDES EXCEPT ACCESS SIDE. PLASTIC LINING TO BE REPLACED WITH EACH OF EACH OF EACH OF THE START OF TH
- EACH CLEANING 4. SIGNS SHALL BE PROVIDED AT THE CONSTRUCTION ENTRANCE AND CONCRETE AREAS INDICATING LOCATION OF WASHOUT AREA. . WASHOUT AREA TO BE ENCLOSED IN CONSTRUCTION FENCE.
- 6. WASHOUT AREAS TO BE ENCLOSED IN CONSTRUCTION FERCE.
 6. WASHOUT AREAS TO BE INSPECTED DAILY TO ENSURE LINER IS INTACT AND ADEQUATE CAPACITY IS AVAILABLE AT ALL TIMES. WASHOUT AREAS SHALL BE INSPECTED IMMEDIATELY AFTER HEAVIER RAINS. DAMAGED OR LEAKING WASHOUT AREAS TO BE DEACTIVATED AND REPAINED IMMEDIATELY.
- 7. CONCRETE WASTE SHALL BE REMOVED AND DISPOSED OF ONCE IT REACHES THREE-QUARTERS OF THE WASHOUT AREA'S HEIGHT. ALL WASTE SHALL BE DISPOSED OF IN A MANNER CONSISTENT WITH APPLICABLE LAWS, REGULATIONS, AND GUIDELINES OF MUNICIPALITY.



✓ 3500# AIR ENTRAINED CONCRETE - 2-#5 REBARS CONTINUOUS

NOTE ALL STUBS TO BE INSTALLED BY MANUFACTURER. OUTLET DETAIL

Posted Speed Limit =	30	mph
Design Speed Limit =	30	mph
Stopping Sight Distance =	200	(ft) design
Height of Driver's Eye =	3.50	(ft)
Ground Elevation =	21.00	(ft)
Driver's Eye Elevation =	24.50	(ft)
Height of Approaching Vehicle =	4.30	(ft)
Ground Elevation 200' North=	11.42	(ft) +/-
Top of Approaching Vehicle =	15.72	(ft) +/-
Ground Elevation 96' West =	20.47	(ft) +/-
Top of Approaching Vehicle =	24.77	(ft) +/-
Ground Elevation 79' Southwest =	21.57	(ft) +/-
Top of Approaching Vehicle =	25.87	(ft) +/-

STORMWATER MANAGEMENT PLAN & DRAINAGE ANALYSIS

7 Bay Avenue Village of Larchmont - New York

December 27, 2017 Revised April 2, 2019

Hudson Engineering & Consulting, P.C.

45 Knollwood Road – Suite 201 Elmsford, NY 10523 (914) 909-0420

STORMWATER MANAGEMENT PLAN & DRAINAGE ANALYSIS 7 Bay Avenue Village of Larchmont - New York

INTRODUCTION

This Stormwater Management Plan presents the proposed Best Management Practices (BMPs) to control erosion and sedimentation and manage stormwater during and upon construction of Proposed dwelling, driveway, pool and patio at 7 Bay Avenue in the Village of Larchmont, Westchester County, New York.

This plan consists of this narrative and a plan set entitled: "Proposed Dwelling, 7 Bay Avenue, Village of Larchmont, Westchester County - New York", all as prepared by Hudson Engineering and Consulting, P.C., Elmsford, New York, last revised April 2, 2019. The design is in accordance with the Village of Larchmont requirements. Since the project disturbance is less than one acre the New York State Department of Environmental Conservation [NYSDEC] stormwater regulations are not applicable.

METHODOLOGY

In accordance with the exemption listed in the Village Code, Section 335-28. (B).(2), "The Stormwater Management Officer may waive or reduce any of the requirements of this section if he/she determines that such existing Village stormwater facility is of adequate size, and will discharge surface water runoff directly to Long Island Sound, the East Creek, or the Premium River without adversely affecting drainage from any other area." Therefore, the stormwater management system shall only be designed for water quality measures and will exclude attenuation.

The stormwater analysis was developed utilizing the Soil Conservation Service (SCS) TR-20, 24-hour Type III storm events (HydroCad®) to assist with the design of the mitigating practices. The "Complex Number" (CN) value determination is based on soil type, vegetation and land use. The design is in accordance with the Village of Larchmont's stormwater regulations. The "Time of Concentration" (T_c) was determined as a direct entry of one-minute. The CN and T_c data are input into the computer model. The project site was modeled for the water quality rainfall event (1.65-inches) Type III – 24-hour storm event. Additionally, an attenuation practice was designed to ensure equivalent or reduced runoff rates up to the 50-year Type III – 24-hour storm events.

PRE-DESIGN INVESTIGATIVE ANALYSIS

A pre-design investigative analysis was performed including deep-hole tests by Soil Testing, Inc. in the locations shown on the plans.

Three (3) deep-hole tests were excavated and labeled TP-1, TP-2, and TP-3, as shown on the plans.

- TP-1 was excavated to a depth of 54-inches. The test revealed topsoil to a depth of 6-inches, dark brown silt with cobbles and boulders to a depth of 44-inches, and partially decomposed bedrock to the invert. Ledge rock was encountered at 54 inches. No groundwater was encountered.
- TP-2 was excavated to a depth of 8-inches. The test revealed topsoil and sand to the invert. Ledge rock was encountered at 8 inches. No groundwater was encountered.
- TP-1 was excavated to a depth of 18-inches. The test revealed topsoil, sand, and gravel to the invert. Ledge rock was encountered at 18 inches. No groundwater was encountered.

The deep test hole log sheet is attached.

PRE-DEVELOPED CONDITION

In the existing conditions the site was modeled as one watershed, Watershed 1 analyzed as follows:

Watershed 1 contains a tributary area of 40,549 square feet. 27,838 square feet is pervious in the form of lawn and landscaping in "D" soils, and 12,711 square feet is impervious in the form of existing house, walkways, driveway, terrace, steps, and walls. The weighted Complex Number (CN) value was calculated as 86 and the Time of Concentration (Tc) was calculated as 6.4 minutes. The stormwater runoff from Watershed 1 originates in the west of the property and flows east towards DP-1, at which point it exits the site onto the Long Island Sound.

Pre-Developed Stormwater Runoff Rates

(cubic feet per second)

Storm Event	1-Year	2-Year	10-Year	25-Year	50-Year
DP-1	1.66	2.21	3.79	5.02	6.16

See drawing WS-M for watershed areas and location of DP-1.

POST-DEVELOPED CONDITION

The project site was modeled as two watersheds in the proposed condition: Watershed 1, and Watershed 1A. Each watershed was analyzed as follows:

Watershed 1 contains a tributary area of 28,616 square feet. 27,544 square feet is pervious in the form of lawn and landscaping in "D" soils, 1,072 square feet is impervious in the form of existing rear walls, existing concrete walk, existing steps, and proposed walls. The weighted Complex Number (CN) value was calculated as 81 and the Time of Concentration (Tc) was calculated as 6.9 minutes. The stormwater runoff from Watershed 1 originates in the west of the property and flows east towards DP-1, at which point it exits the site onto Long Island Sound.

Watershed 1A contains a tributary area of approximately 11,993 square feet. All of which is impervious in the form of the proposed dwelling, terrace, pool, pool deck, and driveway. The weighted Complex Number (CN) value is calculated as 98 and the Time of Concentration (Tc) is a direct entry of 1.0 minute. The runoff from this tributary area is conveyed via a comprehensive drainage system and released into a proposed rain garden located in the eastern corner of the property. The rain garden has a foot print of 842 square feet, is twelve-inches in depth, and has one overflow discharge pipe for controlled release of the collected stormwater into a 20 linear foot 12-inch attenuation gallery. The exfiltration rate of the soil in the rain garden is modeled at a rate 30 inches per hour. This minimal rate does not account for a small amount of evapotranspiration that will naturally occur from the plantings in the rain garden. The system is designed to fully accept (no release) the entire water control volume runoff (1.66-inches rainfall) up to the 1-year storm event for the watershed. The runoff volume for storm events greater than the 1-year storm event is directed to an eight-inch diameter pipe in the floor of the rain garden. This eight-inch diameter pipe collects the runoff and coveys it to a proposed attenuation gallery consisting of 20 LF of 12" HDPE pipe. The gallery outlets into a 24"x24" drain inlet that is equipped with reduced diameter orifice for controlled release of the collected stormwater to the Long Island Sound up to the 50-year storm event.

The total runoff for the post developed condition at DP-1 was modeled for the 1-, 2-, 10-, 25-, and 50-year Type III - 24-hour storm events.

Storm Event	1-Year	2-Year	10-Year	25-Year	50-Year
DP-1	0.89	1.36	3.00	4.13	5.08

Post-Developed Stormwater Runoff Rates

(cubic feet per second)

See drawing WS-M for watershed areas and location of DP-1.

The proposed post-developed conditions for the site reduce or equal the stormwater runoff rates of the pre-developed conditions at design point [DP-1].

SUMMARY OF FLOWS AT DESIGN POINT

The peak rates of runoff from Watershed 1 and Watershed 1A were calculated to be as follows:

Design					
Point	1-Year	2-Year	10-Year	25-Year	50-Year
DP-1					
Pre-[cfs]	1.66	2.21	3.79	5.02	6.16
 Post-[cfs] 	0.89	1.36	3.00	4.13	5.08

WATER QUALITY VOLUME

P=	90%	Rainfall	1.5	-inches					
A _i =	Imperv =	vious Area A _i =	11,993 0.2753	-square feet -acres	:				
A _t =	Tributa	ary Area = A _t =	11,993 0.2753	-square feet -acres					
=	% Impe	ervious =	100.00%						
R _v =	0.05+0.009(I); where I = Percent Impervious written as a percent								
		R _v = R _v =	0.950 0.950	(0.20 n	ninimum)				
WQ _v =	(P x	R _v x A _t) 12	=	0.03269	acre-feet =	1424.17	cubic feet		
		Rainfall =	1.66	-inches \rightarrow	0.03283	acre-feet	OKAY		

CONSTRUCTION PHASE

During the construction phase of the project, a sediment and erosion control plan shall be implemented in accordance with the New York State Department of Environmental Conservation's Best Management Practices (BMP). The primary goals of the sediment and erosion control plan are to prevent the tracking of dirt and mud onto adjacent roads, to prevent mud and silt from entering into existing and proposed drainage facilities, and to protect the receiving waters from contamination during the construction.

During construction, the party responsible for implementing the temporary (during construction) Stormwater Management facilities Maintenance Program will be the owner. Contact information will be filed with the Village.

A New York State Professional Engineer or Certified Professional in Erosion and Sediment Control (P.E. or CPESC) shall conduct an assessment of the site prior to the commencement of construction and certify in an inspection report that the appropriate erosion and sediment controls shown on the plan have been adequately installed and/or implemented to ensure overall preparedness of the site for construction. Following the commencement of construction, site inspections shall be conducted by the P.E. or CPESC at least every 7 calendar days and within 24 hours of the end of a storm event of 0.5 inches or greater.

During each inspection, the representative shall record the following:

- 1. On a site map, indicate the extent of all disturbed site areas and drainage pathways. Indicate site areas that are expected to undergo initial disturbance or significant site work within the next 14-day period;
- 2. Indicate on a site map all areas of the site that have undergone temporary or permanent stabilization;
- 3. Indicate all disturbed site areas that have not undergone active site work during the previous 14-day period;
- 4. Inspect all sediment control practices and record approximate degree of sediment accumulation as a percentage of the sediment storage volume;
- 5. Inspect all erosion and sediment control practices and record all maintenance requirements. Identify any evidence of rill or gully erosion occurring on slopes and any loss of stabilizing vegetation or seeding/mulching. Document any excessive deposition of sediment or ponding water along the barrier. Record the depth of sediment within containment structures and any erosion near outlet and overflow structures.
- 6. All identified deficiencies.

The construction manager shall maintain a record of all inspection reports in a site logbook. The site logbook shall be maintained on-site and be made available to the Village of Larchmont and/or the NYSDEC. A summary of the site inspection activities shall be posted on a monthly basis in a public accessible location at the site.

The projects anticipated start date is Spring 2019 and the anticipated completion date is Summer 2019.

CONSTRUCTION SEQUENCING

The following erosion control schedule shall be utilized:

- 1. Prior to commencing construction, a pre-construction meeting shall be scheduled with the Village.
- 2. Install a stabilized construction entrance at the access point(s) to the site.
- 3. Demarcate the limits of disturbance.
- 4. Establish construction staging area.
- 5. Install tree protection o n trees as noted on plans.
- 6. Selective vegetation removal for silt fence installation.
- 7. Install silt fence down slope of all areas to be disturbed as shown on the plan.
- 8. Remove trees where necessary (clear & grub) for the proposed construction.
- 9. Strip topsoil and stockpile at the locations specified on the plans (up gradient of erosion control measures). Temporarily stabilize topsoil stockpiles (hydroseed during May 1st through October 31st planting season or by covering with a tarpaulin(s) November 1st through April 30th. and install silt fence around toe of slope).
- 10. Demolish any existing site features and/or structures noted as being removed on the construction documents, and dispose of off-site.
- 11. Rough grade disturbed site.
- 12. Excavate and construct foundations for new dwelling.
- 13. Excavate and install washed stone and engineered soil media for rain garden per engineer's recommendations and requirement.

- 14. Fine grade and seed all disturbed areas. Clean paved areas and drain lines. Ensure grass stand is achieved.
- 15. Install 4"-6" topsoil, fine grade, seed the disturbed areas and install landscape plantings. spread salt hay over seeded areas.
- 16. Install and connect all roof drain leaders to rain garden.
- 17. Remove all temporary soil erosion and sediment control measures after the site is stabilized with vegetation (80% uniform density of permanent vegetation).

* Soil erosion and sediment control maintenance must occur weekly and prior to and after every ½" or greater rainfall event.

EROSION AND SEDIMENT CONTROL COMPONENTS

The primary aim of the soil and sediment control measures is to reduce soil erosion from areas stripped of vegetation during and after construction and to prevent silt from reaching the off-site drainage structures and downstream properties. The Sediment and Erosion Control Components are an integral component of the construction sequencing and will be implemented to control sedimentation and re-establish vegetation.

Planned erosion and sedimentation control practices during construction include the installation, inspection and maintenance of the inlet protection, soil stockpile areas, and silt fencing. General land grading practices, including land stabilization and construction sequencing are also integrated into the Sediment and Erosion Control Plan. Dust control is not expected to be a problem due to the relatively limited area of exposure. Should excessive dust be generated, it will be controlled by sprinkling.

All proposed soil erosion and sediment control practices have been designed in accordance with the following publications:

- New York State standards and Specifications for Urban Erosion and Sediment Control, November 2016
- New York State General Permit for Stormwater Discharges, GP-0-15-002 (General permit).
- "Reducing the Impacts of Stormwater Runoff from New Development", as published by the New York State Department of Environmental Conservation (NYSDEC), second edition, April, 1993.

The proposed soil erosion and sediment control devices include the planned erosion control practices outlined below. Maintenance procedures for each erosion control practice have also been outlined below.

• SILT FENCE

Silt fence (geo-textile filter cloth) shall be placed in locations depicted on the approved plans. The purpose of the silt fence is to reduce the velocity of sediment laden stormwater from small drainage areas and to intercept the transported sediment load. In general, silt fence shall be used at the toe of slopes or intermediately within slopes where obvious channel concentration of stormwater is not present.

<u>Maintenance</u>

Silt fencing shall be inspected at a minimum of once per week and prior to and within 24 hours following a rain event ½" or greater. Inspections shall include ensuring that the fence material is tightly secured to the woven wire and the wire is secured to the wood posts. In addition, overlapping filter fabric shall be secured and the fabric shall be maintained a minimum of six (6) inches below grade. In the event that any "bulges" develop in the fence, that section of fence shall be replaced within 24 hours with new fence section. Any sediment build-up against the fence shall be removed within 24 hours and deposited on-site a minimum of 100 feet outside of any wetland or watercourse.

The installation of silt fencing will be maintained or replaced until the fencing is no longer necessary. Once the site is stabilized, all silt fences shall be removed. The immediate area occupied by the silt fence will be shaped to an acceptable grade and stabilized.

• INLET PROTECTION

After catch basins and surface inlets have been installed, these drain inlets will receive stormwater from the roadways, driveways, and surrounding overland watersheds. In order to protect the receiving waters from sedimentation, the contractor shall install stone and block inlet protection as shown on the plans. Once installed, ³/₄ inch stone aggregate shall be installed around the perimeter of all catch basins and surface inlets as illustrated on the approved plans. This barrier will allow stormwater to be filtered prior to reaching the basin inlet grate.

The stone barrier should have a minimum height of 1 foot and a maximum height of 2 feet. Do not use mortar. The height should be limited to prevent excess ponding and bypass flow. Recess the first course of blocks at least 2 inches below the crest opening of the storm drain for lateral support. Subsequent courses can be supported laterally if needed by placing a 2x4 inch wood stud through the block openings perpendicular to the course. The bottom row should have a few blocks oriented so flow can drain through the block to dewater the basin area. The stone should be placed just below the

top of the blocks on slopes of 2:1 or flatter. Place hardware cloth of wire mesh with $\frac{1}{2}$ inch openings over all block openings to hold stone in place.

As an optional design, the concrete blocks may be omitted and the entire structure constructed of stone, ringing the outlet ("doughnut"). The stone should be kept at a 3:1 slope toward the inlet to keep it from being washed into the inlet.

A level area 1 foot wide and four inches below the crest will further prevent wash. Stone on the slope toward the inlet should be at least 3 inches in size for stability and 1 inch or smaller away from the inlet to control flow rate. The elevation of the top of the stone crest must be maintained 6 inches lower than the ground elevation down slope from the inlet to ensure that all storm flows pass over the stone into the storm drain and not past the structure.

The barrier should be inspected after each rain event and repairs made within 24 hours. Remove sediment as necessary to provide for accurate storage volume for subsequent rains. Upon stabilization of contributing drainage area, remove all materials and any unstable soil and dispose of properly. Bring the disturbed area to proper grade, smooth, compact and stabilized in a manner appropriate to the site.

Maintenance

Stone Aggregate: The stone aggregate shall be inspected weekly prior to and within 24 hours following a rain event $\frac{1}{2}$ " or greater. Care shall be taken to ensure that all stone aggregate is properly located and secure and do not become displaced. The stone aggregate shall be inspected for accumulated sediments and any accumulated sediment shall be removed from the device and deposited not less than 100 feet from wetland or watercourse.

• TREE PROTECTION

All significant trees to be preserved located within the limits of disturbance and on the perimeter of the disturbance limits shall be protected from harm by erecting a 3' high (minimum) snow fence completely surrounding the tree. Snow fence should extend to the drip-line of the tree to be preserved. Trees designated to be protected shall be identified during the staking of the limits of disturbance for each construction phase.

<u>Maintenance</u>

The snow fence shall be inspected daily to ensure that the perimeter of the fence remains at the drip-line of the tree to be preserved. Any damaged portions of the fence shall be repaired or replaced within 48 hours. Care shall also be taken to ensure that no construction equipment is driven or parked within the drip-line of the tree to be preserved.

• SOIL/SHOT ROCK STOCKPILING

All soil and shot rock stripped from the construction area during grubbing and mass grading shall be stockpiled in locations shown on the plans, but in no case shall they be placed within 100' of a wetland or watercourse. The stockpiled soils shall be re-used during finish-grading to provide a suitable growing medium for plant establishment. Soil stockpiles shall be protected from erosion by vegetating the stockpile with rapidly –germinating grass seed (during the May 1^{st} – October 30^{th}) planting season or covering the stockpile with tarpaulin the remainder of the year. Install silt fence around toe of slope.

Maintenance

Sediment controls (silt fence) surrounding the stockpiles shall be inspected according to the recommended maintenance outline above. All stockpiles shall be inspected for signs of erosion or problems with seed establishment weekly or tarpaulin and prior to and within 24 hours following a rain event ½" or greater.

• GENERAL LAND GRADING

The intent of the Erosion & Sediment Control Plan is to control disturbed areas such that soils are protected from erosion by temporary methods and, ultimately, by permanent vegetation. Where practicable, all cut and fill slopes shall be kept to a maximum slope of 2:1. In the event that a slope must exceed a 2:1 slope, it will be stabilized with stone riprap. On fill slopes, all material will be placed in layers not to exceed 12 inches in depth and adequately compacted.

• SURFACE STABILIZATION

All disturbed areas will be protected from erosion with the use of vegetative measures (i.e., grass seed mix, sod) hydromulch netting or hay. When activities temporarily cease during construction, soil stockpiles and exposed soil should be stabilized by seed, mulch or other appropriate measures within 7 days after construction activity has ceased, or 24 hours prior to a rain event $\frac{1}{2}$ " or greater.

All seeded areas will be re-seeded areas as necessary and mulched according to the site plan to maintain a vigorous, dense vegetative cover,

Erosion control barriers (silt fencing) shall be placed around exposed areas during construction. Where exposed areas are immediately uphill from a wetland or watercourse, the erosion control barrier will consist of double rows of silt fencing. Any areas stripped of vegetation during construction will be vegetated and/or mulch, but in no case more than 14 days to prevent erosion of the exposed soils. And topsoil removed during construction will be temporarily stockpiled for future use in grading and landscaping.

As mentioned above, temporary vegetation will be established to protect exposed soil areas during construction. If growing conditions are not suitable for the temporary vegetation, mulch will be used to the satisfaction of the Town Engineer. Materials that may be used for mulching include straw, hay, salt hay, wood fiber, synthetic soil stabilizers, mulch netting, sod or hydromulch. In site areas where significant erosion potential exists (steep slopes) and where specifically directed by the Town's representative, Curlex Excelsior erosion control blankets (manufactured by American Excelsior, or approved equal) shall be installed. A permanent vegetative cover will be established upon completion of construction of those areas that have been brought to finish-grade and to remain undisturbed.

• Temporary Stabilization (May 1st through October 31st planting season)

The following seeding application should be used depending on the time of year.

- Spring/summer or early fall, seed the area with ryegrass (annual or perennial) at 30 lbs. per acre (Approximately 0.7 lb/1000 sq. ft. or use 1 lb/1000 sq. ft.).
- Late fall or early winter, seed Certified 'Aroostook' winter rye (cereal rye) at 100 lbs. per acre (2.5 lbs/1000 sq. ft.).
- Permanent Stabilization (May 1st through October 31st planting season)
 - 1. Provide minimum of four (4) inches topsoil for all new lawn areas. Top dress all existing disturbed lawn areas with two (2) inches of topsoil.
 - Grass seed shall be evenly sown by mechanical seeder at a rate of 3.0-4.0 pounds per 1,000 square feet.
 - 3. Fine rake, roll and water to a depth of one inch all seeded areas.
 - Apply air-dried hay or straw mulch to provide 90% coverage of surface (approximately 90 lbs. per 1,000 sf). Use small grain straw where mulch is maintained for more than three months
 - 5. Contractor shall provide, at his own expense, protection against trespassing and other damage to lawn areas.
 - 6. <u>Lawn seed mix</u> shall include:
 - a. General Recreation areas and lawns:

- 65% Kentucky Bluegrass blend
- 20% Perennial Rye
- 15% Fine fescue

Sod may be used as an alternate to seeding in select areas.

Slow release fertilizers will be applied by hand to horticultural plantings as part of regular horticultural maintenance program and shall be limited to a single spring application.

CONSTRUCTION PRACTICES TO MINIMIZE STORMWATER CONTAMINATION

Adequate measures shall be taken to minimize contaminant particles arising from the discharge of solid materials, including building materials, grading operations, and the reclamation and placement of pavement, during project construction, including but not limited to:

- Building materials, garbage, and debris shall be cleaned up daily and deposited into dumpsters, which will be periodically removed from the site and appropriately disposed of.
- Dump trucks hauling material from the construction site will be covered with a tarpaulin.
- The paved street adjacent to the site entrance will be swept daily to remove excess mud, dirt, or rock tracked from the site.
- Petroleum products will be stored in tightly sealed containers that are clearly labeled.
- All vehicles on site will be monitored for leaks and receive regular preventive maintenance to reduce the chance of leakage.
- All spills will be cleaned up immediately upon discovery. Spills large enough to reach the storm system will be reported to the National Response Center at 1-800-424-8802.
- Materials and equipment necessary for spill cleanup will be kept in the temporary material storage trailer onsite. Equipment will include, but not be limited to, brooms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, saw dust, and plastic and metal trash containers.
- All paint containers and curing compounds will be tightly sealed and stored when not required for use. Excess paint will not be discharged to the storm system, but will be properly disposed according to the manufacturer's instructions.

- Sanitary waste will be collected from portable units a minimum of two times a week to avoid overfilling.
- Any asphalt substances used on-site will be applied according to the manufacturer's recommendation.
- Fertilizers will be stored in a covered shed and partially used bags will be transferred to a sealable bin to avoid spills and will be applied only in the minimum amounts recommended by the manufacturer and worked into the soil to limit exposure to stormwater.
- No disturbed area shall be left un-stabilized for longer than 14 days during the growing season.
- When erosion is likely to be a problem, grubbing operations shall be scheduled and performed such that grading operations and permanent erosion control features can follow within 24 hours thereafter.
- As work progresses, patch seeding shall be done as required on areas previously treated to maintain or establish protective cover.
- Drainage pipes and swales/ditches shall generally be constructed in a sequence from outlet to inlet in order to stabilize outlet areas and ditches before water is directed to the new installation or any portion thereof, unless conditions unique to the location warrant an alternative method.

STORMWATER MANAGEMENT FACILITIES MAINTENANCE PROGRAM

The following maintenance plan has been developed to maintain the proper function of all drainage and erosion and sediment control facilities:

- Minimize the use of road salt for maintenance of driveway areas.
- Drainage inlets/structures shall be vacuum swept twice a year, at the conclusion of the landscape season in the fall and at the conclusion of the sand and de-icing season in the spring.
- <u>General Stormwater Facilities Maintenance (Storm Sewer, Catch</u> <u>Basins/Drain Inlets, Manholes, Pre-treatment Device and Subsurface</u> <u>Infiltration System)</u>

All stormwater facilities shall be inspected immediately after completion of construction, and then monthly for the first three (3) months following the completion of the Project. Within the first three (3) months, inspections shall immediately be performed following a large storm event (i.e. producing 1/2"

(one-half inch) of rain or greater. Thereafter, these facilities shall be inspected as described as follows. Upon inspection, facilities shall be immediately maintained and/or cleaned as may be required. Any site areas exhibiting soil erosion of any kind shall be immediately restored and stabilized with vegetation, mulch or stone, depending on the area to be stabilized.

Upon each inspection, all visible debris including, but not limited to, twigs, leaf and forest litter shall be removed from the swales, overflow discharge points and frames and grates of drainage structures.

• Subsurface Attenuation/Exfiltration Gallery:

The subsurface infiltration chambers shall be inspected immediately after construction. Thereafter, the attenuation/exfiltration gallery shall be inspected every six (6) months (Spring and Fall) for excess sediment accumulation. During dry weather conditions, when sediment has accumulated to an average depth exceeding 3" (three inches), the gallery shall be water jetted clean, and all accumulated sediments shall be vacuumed out or removed manually. A stadia rod may be inserted to determine the depth of the sediment.

• <u>Sumps – Catch Basin/Drain Inlets and Drain Manholes</u>

All catch basin/drain inlets and drain manholes with sumps have been designed to trap sediment prior to its transport to the infiltration practice and, ultimately, downstream. These sumps will require periodic inspection and maintenance to ensure that adequate depth is maintained within the sumps.

All sumps shall be inspected once per month for the first three (3) months (after drainage system has been put into service). Thereafter, all sumps shall be inspected every four (4) months. The Owner, or their duly authorized representative, shall take measurements of the sump depth.

If sediment has accumulated to 1/2 (one-half) the depth of the sump, all sediment shall be removed from the sump. Sediments can be removed with hand-labor or with a vacuum truck.

The use of road salt shall be minimized for maintenance of roadway and driveway areas.

The permanent maintenance program will be managed by the future homeowners upon completion of construction and acceptance of the improvements.

CONCLUSION

The stormwater management plan proposed meets all the requirements set forth by the Village of Larchmont. Design modification requirements that may occur during the approval process will be performed and submitted for review to the Village of Larchmont.

Soils Maps & Soils Data

Web Soil Survey National Cooperative Soil Survey
Hydrologic Soil Group—Westchester County, New York (7 Bay Avenue)





Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
CrC	Charlton-Chatfield complex, 0 to 15 percent slopes, very rocky	В	0.4	4.8%
UIC	Urban land-Charlton- Chatfield complex, rolling, very rocky		5.3	68.8%
UpB	Urban land-Paxton complex, 3 to 8 percent slopes	D	0.2	2.1%
W	Water		1.8	24.2%
Totals for Area of Intere	est	7.6	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Aggregation is the process by which a set of component attribute values is reduced to a single value that represents the map unit as a whole.

A map unit is typically composed of one or more "components". A component is either some type of soil or some nonsoil entity, e.g., rock outcrop. For the attribute being aggregated, the first step of the aggregation process is to derive one attribute value for each of a map unit's components. From this set of component attributes, the next step of the aggregation process derives a single value that represents the map unit as a whole. Once a single value for each map unit is derived, a thematic map for soil map units can be rendered. Aggregation must be done because, on any soil map, map units are delineated but components are not.

For each of a map unit's components, a corresponding percent composition is recorded. A percent composition of 60 indicates that the corresponding component typically makes up approximately 60% of the map unit. Percent composition is a critical factor in some, but not all, aggregation methods.

The aggregation method "Dominant Condition" first groups like attribute values for the components in a map unit. For each group, percent composition is set to the sum of the percent composition of all components participating in that group. These groups now represent "conditions" rather than components. The attribute value associated with the group with the highest cumulative percent composition is returned. If more than one group shares the highest cumulative percent composition, the corresponding "tie-break" rule determines which value should be returned. The "tie-break" rule indicates whether the lower or higher group value should be returned in the case of a percent composition tie. The result returned by this aggregation method represents the dominant condition throughout the map unit only when no tie has occurred.

Component Percent Cutoff: None Specified

Components whose percent composition is below the cutoff value will not be considered. If no cutoff value is specified, all components in the database will be considered. The data for some contrasting soils of minor extent may not be in the database, and therefore are not considered.

Tie-break Rule: Higher

The tie-break rule indicates which value should be selected from a set of multiple candidate values, or which value should be selected in the event of a percent composition tie.

Watershed Maps



Pre-Development Analysis of the 1-, 2-, 10-, 25- and 50-year Storm Frequencies



Existing Condition - 2019-03-14	Type III 24-hr
Prepared by Hudson Engineering & Consulting, P.C.	
HydroCAD® 10.00-14 s/n 02549 © 2015 HydroCAD Software Solutions	LLC

1-Year Rainfall=2.86" Printed 3/15/2019 Page 2

Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX: Watershed 1 Runoff Area=40,549 sf 31.35% Impervious Runoff Depth=1.54" Flow Length=81' Slope=0.0352 '/' Tc=6.4 min CN=86 Runoff=1.66 cfs 5,215 cf

Reach ExR: Long Island Sound

Inflow=1.66 cfs 5,215 cf Outflow=1.66 cfs 5,215 cf

Total Runoff Area = 40,549 sf Runoff Volume = 5,215 cf Average Runoff Depth = 1.54" 68.65% Pervious = 27,838 sf 31.35% Impervious = 12,711 sf

Summary for Subcatchment EX: Watershed 1

Runoff = 1.66 cfs @ 12.09 hrs, Volume= 5,215 cf, Depth= 1.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

	A	rea (sf)	CN	Description					
*		994	98	Existing rea	ar walls, wa	lk, steps			
*		74	98	Spa & wall					
*		218	98	Gravel Bed	& walk				
*		1,166	98	Terrace & S	Steps				
*		5,048	98	House & ch	imney				
*		182	98	Walk & ste	os				
*		5,029	98	Walk & driv	eway				
		27,838	80	>75% Grass cover, Good, HSG D					
		40,549	86	86 Weighted Average					
		27,838		68.65% Pei	vious Area				
		12,711		31.35% Imp	pervious Are	ea			
	Тс	Length	Slope	e Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)				
	6.4	81	0.0352	2 0.21		Sheet Flow, A->DP-1			
						Grass: Short n= 0.150	P2= 3.45"		

Summary for Reach ExR: Long Island Sound

Inflow A	\rea =	40,549 sf,	31.35% lm	pervious,	Inflow Depth =	1.54"	for 1-	Year event
Inflow	=	1.66 cfs @	12.09 hrs, \	Volume=	5,215 cf			
Outflow	/ =	1.66 cfs @	12.09 hrs, \	Volume=	5,215 cf	, Atten=	= 0%,	Lag= 0.0 min

Type III 24-hr 2-Year Rainfall=3.45" Printed 3/15/2019 LLC Page 4

Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX: Watershed 1 Runoff Area=40,549 sf 31.35% Impervious Runoff Depth=2.05" Flow Length=81' Slope=0.0352 '/' Tc=6.4 min CN=86 Runoff=2.21 cfs 6,941 cf

Reach ExR: Long Island Sound

Inflow=2.21 cfs 6,941 cf Outflow=2.21 cfs 6,941 cf

Total Runoff Area = 40,549 sf Runoff Volume = 6,941 cf Average Runoff Depth = 2.05" 68.65% Pervious = 27,838 sf 31.35% Impervious = 12,711 sf

Summary for Subcatchment EX: Watershed 1

Runoff = 2.21 cfs @ 12.09 hrs, Volume= 6,941 cf, Depth= 2.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.45"

	A	rea (sf)	CN	Description				
*		994	98	Existing rea	ar walls, wa	lk, steps		
*		74	98	Spa & wall		·		
*		218	98	Gravel Bed	& walk			
*		1,166	98	Terrace & S	Steps			
*		5,048	98	House & ch	imney			
*		182	98	Walk & ste	os			
*		5,029	98	Walk & driv	reway			
		27,838	80	>75% Grass cover, Good, HSG D				
		40,549	86	Weighted Average				
		27,838		68.65% Pei	rvious Area			
		12,711		31.35% Imp	pervious Are	ea		
	Tc	Length	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)			
	6.4	81	0.0352	2 0.21		Sheet Flow, A->DP-1		
						Grass: Short n= 0.150	P2= 3.45"	

Summary for Reach ExR: Long Island Sound

Inflow A	rea =	40,549 sf,	31.35% Impervious,	Inflow Depth = 2.05"	for 2-Year event
Inflow	=	2.21 cfs @	12.09 hrs, Volume=	6,941 cf	
Outflow	=	2.21 cfs @	12.09 hrs, Volume=	6,941 cf, Atter	n= 0%, Lag= 0.0 min

 Type III 24-hr
 10-Year Rainfall=5.12"

 Printed
 3/15/2019

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX: Watershed 1 Runoff Area=40,549 sf 31.35% Impervious Runoff Depth=3.58" Flow Length=81' Slope=0.0352 '/' Tc=6.4 min CN=86 Runoff=3.79 cfs 12,094 cf

Reach ExR: Long Island Sound

Inflow=3.79 cfs 12,094 cf Outflow=3.79 cfs 12,094 cf

Total Runoff Area = 40,549 sf Runoff Volume = 12,094 cf Average Runoff Depth = 3.58" 68.65% Pervious = 27,838 sf 31.35% Impervious = 12,711 sf

Summary for Subcatchment EX: Watershed 1

Runoff = 3.79 cfs @ 12.09 hrs, Volume= 12,094 cf, Depth= 3.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.12"

	A	rea (sf)	CN	Description				
*		994	98	Existing rea	ar walls, wa	lk, steps		
*		74	98	Spa & wall		•		
*		218	98	Gravel Bed	& walk			
*		1,166	98	Terrace & S	Steps			
*		5,048	98	House & ch	imney			
*		182	98	Walk & ste	os			
*		5,029	98	Walk & driv	eway			
		27,838	80	>75% Grass cover, Good, HSG D				
		40,549	86	Weighted Average				
		27,838		68.65% Pei	vious Area			
		12,711		31.35% Imp	pervious Are	ea		
	Tc	Length	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)			
	6.4	81	0.0352	0.21		Sheet Flow, A->DP-1		
						Grass: Short n= 0.150	P2= 3.45"	

Summary for Reach ExR: Long Island Sound

Inflow A	rea =		40,549 sf,	31.35% In	npervious,	Inflow Depth =	3.58" f	or 10	0-Year event
Inflow	=	3	3.79 cfs @	12.09 hrs,	Volume=	12,094 cf			
Outflow	=	3	3.79 cfs @	12.09 hrs,	Volume=	12,094 cf,	, Atten=	0%,	Lag= 0.0 min

 Type III 24-hr
 25-Year Rainfall=6.41"

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX: Watershed 1 Runoff Area=40,549 sf 31.35% Impervious Runoff Depth=4.80" Flow Length=81' Slope=0.0352 '/' Tc=6.4 min CN=86 Runoff=5.02 cfs 16,220 cf

Reach ExR: Long Island Sound

Inflow=5.02 cfs 16,220 cf Outflow=5.02 cfs 16,220 cf

Total Runoff Area = 40,549 sf Runoff Volume = 16,220 cf Average Runoff Depth = 4.80" 68.65% Pervious = 27,838 sf 31.35% Impervious = 12,711 sf

Summary for Subcatchment EX: Watershed 1

Runoff = 5.02 cfs @ 12.09 hrs, Volume= 16,220 cf, Depth= 4.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	A	rea (sf)	CN	Description				
*		994	98	Existing rea	ar walls, wa	lk, steps		
*		74	98	Spa & wall				
*		218	98	Gravel Bed	& walk			
*		1,166	98	Terrace & S	Steps			
*		5,048	98	House & ch	imney			
*		182	98	Walk & ste	os			
*		5,029	98	Walk & driv	eway			
		27,838	80	>75% Gras	s cover, Go	ood, HSG D		
		40,549	86	86 Weighted Average				
		27,838		68.65% Pei	vious Area			
		12,711		31.35% Imp	pervious Are	ea		
	Tc	Length	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	6.4	81	0.0352	. 0.21		Sheet Flow, A->DP-1		
						Grass: Short n= 0.150	P2= 3.45"	

Summary for Reach ExR: Long Island Sound

Inflow A	rea =	40,549 sf,	31.35% Impervious,	Inflow Depth = 4.80"	for 25-Year event
Inflow	=	5.02 cfs @	12.09 hrs, Volume=	16,220 cf	
Outflow	=	5.02 cfs @	12.09 hrs, Volume=	16,220 cf, Atte	en= 0%, Lag= 0.0 min

 Type III 24-hr
 50-Year Rainfall=7.60"

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Time span=0.00-60.00 hrs, dt=0.01 hrs, 6001 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EX: Watershed 1 Runoff Area=40,549 sf 31.35% Impervious Runoff Depth=5.94" Flow Length=81' Slope=0.0352 '/' Tc=6.4 min CN=86 Runoff=6.16 cfs 20,086 cf

Reach ExR: Long Island Sound

Inflow=6.16 cfs 20,086 cf Outflow=6.16 cfs 20,086 cf

Total Runoff Area = 40,549 sf Runoff Volume = 20,086 cf Average Runoff Depth = 5.94" 68.65% Pervious = 27,838 sf 31.35% Impervious = 12,711 sf

Summary for Subcatchment EX: Watershed 1

Runoff = 6.16 cfs @ 12.09 hrs, Volume= 20,086 cf, Depth= 5.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=7.60"

	A	rea (sf)	CN	Description				
*		994	98	Existing rea	ar walls, wa	lk, steps		
*		74	98	Spa & wall		·		
*		218	98	Gravel Bed	& walk			
*		1,166	98	Terrace & S	Steps			
*		5,048	98	House & ch	imney			
*		182	98	Walk & ste	os			
*		5,029	98	Walk & driv	reway			
		27,838	80	>75% Grass cover, Good, HSG D				
		40,549	86	Weighted Average				
		27,838		68.65% Pei	rvious Area			
		12,711		31.35% Imp	pervious Are	ea		
	Tc	Length	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)			
	6.4	81	0.0352	2 0.21		Sheet Flow, A->DP-1		
						Grass: Short n= 0.150	P2= 3.45"	

Summary for Reach ExR: Long Island Sound

Inflow A	rea =	40,549 sf,	31.35% Imperviou	s, Inflow Depth = 5	.94" for 50-Year event
Inflow	=	6.16 cfs @	12.09 hrs, Volume	= 20,086 cf	
Outflow	=	6.16 cfs @	12.09 hrs, Volume	= 20,086 cf,	Atten= 0%, Lag= 0.0 min

Post-Development Analysis of the 1-, 2-, 10-, 25- and 50-year Storm Frequencies



Proposed Condition - 2019-03-27		Туре	III 24-hr 1-	Year Rainfa	nll=2.86"
Prepared by Hudson Engineering & Consu	lting, P.C.			Printed 4	4/2/2019
HydroCAD® 10.00-14 s/n 02549 © 2015 HydroC	AD Software Sol	utions LLC			Page 2
Time span=0.00-60 Runoff by SCS TR-2 Reach routing by Stor-Ind+Tran	0.00 hrs, dt=0.01 0 method, UH=5 is method - Poi	l hrs, 6001 p SCS, Weigh nd routing b	ooints ted-CN y Stor-Ind m	nethod	
Subcatchment 1: Watershed 1 Flow Length=92' S	Runoff Area=28, Slope=0.0370 '/'	616 sf 3.75 ^c Tc=6.9 min	% Imperviou CN=81 Ru	s Runoff Dep noff=0.89 cfs	oth=1.21" 2,878 cf
Subcatchment 1A: Watershed 1A Ru	unoff Area=11,93	3 sf 100.00 ⁰ Tc=1.0 min	% Imperviou CN=98 Ru	s Runoff Dep noff=0.90 cfs	oth=2.63" 2,614 cf
Reach 1R: Long Island Sound			In Out	flow=0.89 cfs flow=0.89 cfs	2,878 cf 2,878 cf
Pond 1P: Rain Garden Discarded=0.42	Peak Elev=1 cfs 2,615 cf Pr	2.46' Storag imary=0.00 c	e=230 cf In fs 0 cf Out	flow=0.90 cfs flow=0.42 cfs	2,614 cf 2,615 cf
Pond 2P: 20 Linear Feet 1.0-Foot Diameter H	DPE Peak	k Elev=9.00'	Storage=0 c	f Inflow=0.00 Outflow=0.00) cfs 0 cf) cfs 0 cf
Total Runoff Area = 40,549 sf 67.9	Runoff Volum 93% Pervious =	e = 5,492 cf 27,544 sf	Average l 32.07% Im	Runoff Deptl pervious = 1	n = 1.63" 3,005 sf

Summary for Subcatchment 1: Watershed 1

Runoff = 0.89 cfs @ 12.10 hrs, Volume= 2,878 cf, Depth= 1.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

	A	rea (sf)	CN	Description					
*		994	98	Existing rea	ar walls, wa	lk, steps			
*		78	98	Spa & wall					
		27,544	80	>75% Gras	•75% Grass cover, Good, HSG D				
		28,616	81	81 Weighted Average					
		27,544		96.25% Pervious Area					
		1,072		3.75% Impe	ervious Area	а			
(Tc min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description			
	6.9	92	0.0370	0.22		Sheet Flow, A->DP-1 Grass: Short n= 0.150	P2= 3.45"		

Summary for Subcatchment 1A: Watershed 1A

Runoff = 0.90 cfs @ 12.01 hrs, Volume= 2,614 cf, Depth= 2.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-Year Rainfall=2.86"

	Area (sf)	CN	Description				
*	2,464	98	Pool & Poo	l deck			
*	5,322	98	Proposed F	Residence			
*	980	98	Proposed T	errace			
*	3,167	98	Proposed D	Driveway			
	11,933	98	Weighted A	verage			
	11,933		100.00% In	100.00% Impervious Area			
T (mir	c Length 1) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description		
1.	0				Direct Entry, Direct Entry		

Summary for Reach 1R: Long Island Sound

Inflow Are	a =	40,549 sf,	32.07% Impervious,	Inflow Depth = 0.85"	for 1-Year event
Inflow	=	0.89 cfs @	12.10 hrs, Volume=	2,878 cf	
Outflow	=	0.89 cfs @	12.10 hrs, Volume=	2,878 cf, Atter	n= 0%, Lag= 0.0 min

Summary for Pond 1P: Rain Garden

Inflow Area	= 11,933	sf,100.00% Impervic	ous, Inflow Depth = 2.	63" for 1-Year event
Inflow	= 0.90 cfs (😥 12.01 hrs, Volum	e= 2,614 cf	
Outflow	= 0.42 cfs (d	🖞 12.11 hrs, Volum	e= 2,615 cf.	Atten= 54%, Lag= 5.6 min
Discarded	= 0.42 cfs (2 12.11 hrs. Volum	e= 2.615 cf	ý č
Primary	= 0.00 cfs ($0.00 \mathrm{hrs}$ Volum	e= 0 cf	
Routing by	Stor-Ind method	Time Span= 0 00-60	00 hrs dt = 0.01 hrs / 3	
Peak Elev=	12 46' @ 12 11 h	rs Surf Area= 601 s	f Storage = 230 cf	
Plug-Flow c	letention time= (no	ot calculated: outflow	precedes inflow)	
Center_of_M	lass det time= 2.3	$2 \min(756.4 - 754.2)$		
Ochici-ol-iv		2 11111 (7 30.4 - 7 34.2)	
Volume	Invert Avai	l Storage Storage I	Description	
		i e te ta ge		
1 1	12 00'	618 cf Custom	Stano Data (Prismatic)	Listed helow (Recalc)
#1	12.00'	618 cf Custom	Stage Data (Prismatic)	Listed below (Recalc)
#1 Elevation	12.00' Surf Area	618 cf Custom	Stage Data (Prismatic)	Listed below (Recalc)
#1 Elevation (feet)	12.00' Surf.Area (sq-ft)	618 cf Custom Inc.Store (cubic-feet)	Stage Data (Prismatic) Cum.Store (cubic-feet)	Listed below (Recalc)
#1 Elevation (feet)	12.00' Surf.Area (sq-ft) 204	618 cf Custom Inc.Store (cubic-feet)	Stage Data (Prismatic) Cum.Store (cubic-feet)	Listed below (Recalc)
#1 Elevation (feet) 12.00	12.00' Surf.Area (sq-ft) 394	618 cf Custom Inc.Store (cubic-feet) 0	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 619	Listed below (Recalc)
#1 Elevation (feet) 12.00 13.00	12.00' Surf.Area (sq-ft) 394 842	618 cf Custom Inc.Store (cubic-feet) 0 618	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 618	Listed below (Recalc)
#1 Elevation (feet) 12.00 13.00	12.00' Surf.Area (sq-ft) 394 842	618 cf Custom Inc.Store (cubic-feet) 0 618	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 618	Listed below (Recalc)
#1 Elevation (feet) 12.00 13.00 Device Ro	12.00' Surf.Area (sq-ft) 394 842 puting In	618 cf Custom Inc.Store (cubic-feet) 0 618 vert Outlet Devices	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 618	Listed below (Recalc)
#1 Elevation (feet) 12.00 13.00 Device Ro #1 Di	12.00' Surf.Area (sq-ft) 394 842 buting In scarded 12	618 cf Custom Inc.Store (cubic-feet) 0 618 vert Outlet Devices .00' 30.000 in/hr E	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 618 xfiltration over Surface	e area
#1 Elevation (feet) 12.00 13.00 Device Ro #1 Di #2 Pr	12.00' Surf.Area (sq-ft) 394 842 buting In scarded 12 imary 12	618 cf Custom Inc.Store (cubic-feet) 0 618 vert Outlet Devices .00' 30.000 in/hr E .50' 8.0'' Horiz. Or	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 618 stiltration over Surface fice/Grate C= 0.600	Listed below (Recalc) e area Limited to weir flow at low heads
#1 Elevation (feet) 12.00 13.00 Device Ro #1 Di #2 Pr	12.00' Surf.Area (sq-ft) 394 842 buting In scarded 12 imary 12	618 cf Custom Inc.Store (cubic-feet) 0 618 vert Outlet Devices .00' 30.000 in/hr E .50' 8.0'' Horiz. Ori	Stage Data (Prismatic) Cum.Store (cubic-feet) 0 618 stiltration over Surface fice/Grate C= 0.600	e area Limited to weir flow at low heads

1=Exfiltration (Exfiltration Controls 0.42 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=12.00' (Free Discharge) ←2=Orifice/Grate (Controls 0.00 cfs)

ry for Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE [Solid] 2.5-Inch Orifice @ 9.0 FT, 8.0-Inch Orifice @

Inflow Area	a =	11,933 sf,1	00.00% Impervious,	Inflow Depth = 0.00"	for 1-Year event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 9.00' @ 0.00 hrs Surf.Area= 4 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	9.00'	16 cf	12.0" Round Pipe Storage
			L= 20.0'
#2	9.00'	10 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		26 cf	Total Available Storage

Proposed Condition - 2019-03-27

Type III 24-hr 1-Year Rainfall=2.86" Printed 4/2/2019 Page 5

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Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
9.0	00	4	0	0		
11.5	50	4	10	10		
Device	Routing	Invert	Outlet Devices			
#1	Primary	9.00'	2.5" Vert. Orific	e/Grate C= 0.6	300	
#2	Primary	9.92'	8.0" Vert. Orific	e/Grate C= 0.6	300	
Primary	OutFlow	Max=0.00 cfs (@ 0.00 hrs HW=	9.00' (Free Disc	harge)	

1=Orifice/Grate (Controls 0.00 cfs) 2=Orifice/Grate (Controls 0.00 cfs)

Proposed Condition - 2019-03-27	Type III 24-hr 2-Year Rainfall=3.45"
Prepared by Hudson Engineering & Consulting, P.C.	Printed 4/2/2019
HydroCAD® 10.00-14 s/n 02549 © 2015 HydroCAD Software So	olutions LLC Page 6
Time span=0.00-60.00 hrs, dt=0.0 Runoff by SCS TR-20 method, UH= Reach routing by Stor-Ind+Trans method - P)1 hrs, 6001 points =SCS, Weighted-CN ond routing by Stor-Ind method
Subcatchment 1: Watershed 1 Runoff Area=28 Flow Length=92' Slope=0.0370 '/'	3,616 sf 3.75% Impervious Runoff Depth=1.67" Tc=6.9 min CN=81 Runoff=1.24 cfs 3,978 cf
Subcatchment 1A: Watershed 1A Runoff Area=11,9	33 sf 100.00% Impervious Runoff Depth=3.22" Tc=1.0 min CN=98 Runoff=1.10 cfs 3,199 cf
Reach 1R: Long Island Sound	Inflow=1.36 cfs 4,038 cf Outflow=1.36 cfs 4,038 cf
Pond 1P: Rain Garden Peak Elev= Discarded=0.46 cfs 3,139 cf Pr	12.58' Storage=307 cf Inflow=1.10 cfs 3,199 cf imary=0.17 cfs 60 cf Outflow=0.62 cfs 3,198 cf
Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE Peak	Elev=9.69' Storage=14 cf Inflow=0.17 cfs 60 cf Outflow=0.13 cfs 60 cf
Total Runoff Area = 40,549 sf Runoff Volu 67.93% Pervious	me = 7,177 cf Average Runoff Depth = 2.12" = 27,544 sf 32.07% Impervious = 13,005 sf

Summary for Subcatchment 1: Watershed 1

Runoff = 1.24 cfs @ 12.10 hrs, Volume= 3,978 cf, Depth= 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.45"

	A	rea (sf)	CN	Description					
*		994	98	Existing rea	r walls, wa	lk, steps			
*		78	98	Spa & wall	Spa & wall				
		27,544	80	>75% Gras	75% Grass cover, Good, HSG D				
		28,616	81	Weighted Average					
		27,544		96.25% Pervious Area					
		1,072		3.75% Impe	ervious Area	а			
(1	Tc min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description			
	6.9	92	0.0370	0.22		Sheet Flow, A->DP-1 Grass: Short n= 0.150	P2= 3.45"		

Summary for Subcatchment 1A: Watershed 1A

Runoff = 1.10 cfs @ 12.01 hrs, Volume= 3,199 cf, Depth= 3.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 2-Year Rainfall=3.45"

	Area (sf)	CN	Description				
*	2,464	98	Pool & Poo	l deck			
*	5,322	98	Proposed F	Residence			
*	980	98	Proposed T	errace			
*	3,167	98	Proposed D	Proposed Driveway			
	11,933	98	Weighted Average				
	11,933		100.00% In	npervious A	rea		
T (min	c Length	Slop	e Velocity	Capacity	Description		
		(101		(015)			
1.	0				Direct Entry, Direct Entry		

Summary for Reach 1R: Long Island Sound

Inflow Are	a =	40,549 sf,	32.07% Impervious,	Inflow Depth = 1.19"	for 2-Year event
Inflow	=	1.36 cfs @	12.11 hrs, Volume=	4,038 cf	
Outflow	=	1.36 cfs @	12.11 hrs, Volume=	4,038 cf, Atte	en= 0%, Lag= 0.0 min

Proposed Condition - 2019-03-27 Prepared by Hudson Engineering & Consulting, P.C.

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Summary for Pond 1P: Rain Garden

Inflow Area	a = 11	,933 sf,100.	00% Impervious	, Inflow Depth = 3.22	2" for 2-Year event
Inflow	= 1.10	cfs @ 12.0	1 hrs, Volume=	3,199 cf	
Outflow	= 0.62	cfs @ 12.0	9 hrs, Volume=	3,198 cf, At	ten= 43%, Lag= 4.5 min
Discarded	= 0.46	cfs @ 12.0	9 hrs, Volume=	: 3,139 cf	-
Primary	= 0.17	cfs @ 12.0	9 hrs, Volume=	= 60 cf	
Routing by	Stor-Ind met	nod, Time Sp	oan= 0.00-60.00	hrs, dt= 0.01 hrs / 3	
Peak Elev	= 12.58' @ 12	.09 hrs Sur	f.Area= 656 sf	Storage= 307 cf	
Plug-Flow	detention time	= 2.7 min ca	alculated for 3,1	98 cf (100% of inflow)	
Center-of-	Mass det. time	e= 2.7 min (752.9 - 750.2)		
Volumo	Invert	Avail Stores	e Staraga Da	aarintian	
volume	Invert	Avail.Storag	je Storage De	scription	
#1	12.00'	618	cf Custom Sta	age Data (Prismatic) ∟	isted below (Recalc)
Flovation			Ino Store	Cum Store	
(foot)	Sull.P	liea	Inc.Store	Culli.Slore	
(100)		∼ft) (o	ubia faat)	(oubic foot)	
(1001)	(50	<u>q-ft) (c</u>	ubic-feet)	(cubic-feet)	
12.00	(50	q-ft) (c 394	ubic-feet) 0	(cubic-feet) 0	
12.00 13.00	(50	<u>q-ft) (c</u> 394 842	ubic-feet) 0 618	<u>(cubic-feet)</u> 0 618	
12.00 13.00	(Si	<u>q-ft) (c</u> 394 842	ubic-feet) 0 618	<u>(cubic-feet)</u> 0 618	
12.00 13.00 Device F	Routing	<u>q-ft) (c</u> 394 842 Invert (ubic-feet) 0 618 Dutlet Devices	(cubic-feet) 0 618	
<u>12.00</u> 13.00 <u>Device F</u> #1 C	(Si Routing Discarded	<u>q-ft) (c</u> 394 842 <u>Invert (c</u> 12.00' 3	ubic-feet) 0 618 Dutlet Devices 0.000 in/hr Exfi	(cubic-feet) 0 618 Itration over Surface a	area
<u>12.00</u> 13.00 <u>Device F</u> #1 E #2 F	(Souting Discarded Primary	q-ft) (c 394 842 <u>Invert (</u> 12.00' 3 12.50' 8	ubic-feet) 0 618 Dutlet Devices 0.000 in/hr Exfi .0" Horiz. Orific	(cubic-feet) 0 618 Itration over Surface a ce/Grate C= 0.600 L	area .imited to weir flow at low heads

Discarded OutFlow Max=0.46 cfs @ 12.09 hrs HW=12.58' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.46 cfs)

Primary OutFlow Max=0.17 cfs @ 12.09 hrs HW=12.58' (Free Discharge) **2=Orifice/Grate** (Weir Controls 0.17 cfs @ 0.95 fps)

ry for Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE [Solid] 2.5-Inch Orifice @ 9.0 FT, 8.0-Inch Orifice @

Inflow Area	a =	11,933 sf	,100.00% Impervious,	Inflow Depth =	0.06" f	or 2-Year event
Inflow	=	0.17 cfs @	12.09 hrs, Volume=	60 cf		
Outflow	=	0.13 cfs @	12.12 hrs, Volume=	60 cf,	, Atten=	26%, Lag= 2.0 min
Primary	=	0.13 cfs @	12.12 hrs, Volume=	60 cf		

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 9.69' @ 12.12 hrs Surf.Area= 23 sf Storage= 14 cf

Plug-Flow detention time= 1.6 min calculated for 60 cf (100% of inflow) Center-of-Mass det. time= 1.6 min (728.2 - 726.7)

Volume	Invert	Avail.Storage	Storage Description
#1	9.00'	16 cf	12.0" Round Pipe Storage
			L= 20.0'
#2	9.00'	10 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		26 cf	Total Available Storage

Proposed Condition - 2019-03-27

Type III 24-hr 2-Year Rainfall=3.45" Printed 4/2/2019 Page 9

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Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
9.00		4	0	0		
11.5	11.50 4		10	10		
Device	Routing	Invert	Outlet Devices			
#1	Primary	9.00'	2.5" Vert. Orific	e/Grate C=	0.600	
#2	Primary	9.92'	8.0" Vert. Orific	e/Grate C=	0.600	

Primary OutFlow Max=0.12 cfs @ 12.12 hrs HW=9.68' (Free Discharge) -1=Orifice/Grate (Orifice Controls 0.12 cfs @ 3.66 fps) -2=Orifice/Grate (Controls 0.00 cfs)

Proposed Condition - 2019-03-27		Type III 24-hr	10-Year Rainfall=5.12"
Prepared by Hudson Engineering & C	onsulting, P.C.		Printed 4/2/2019
HydroCAD® 10.00-14 s/n 02549 © 2015 H	ydroCAD Software Solutio	ns LLC	Page 10
Time and a O	00 00 00 has de-0 04 has	- 0001 m sints	
Time span=0.	UU-60.00 nrs, dt=0.01 nr	s, 6001 points	
Reach routing by Stor-Ind-	+Trans method - Pondu	routing by Stor-li	nd method
reach routing by otor-ind			la metrioa
Subcatchment 1: Watershed 1	Runoff Area=28,616	sf 3.75% Imper	vious Runoff Depth=3.09"
Flow Length=	92' Slope=0.0370 '/' Tc=	=6.9 min CN=81	Runoff=2.30 cfs 7,372 cf
Subcatchment 1A: Watershed 1A	Runoff Area=11,933 sf	f 100.00% Imper	vious Runoff Depth=4.88"
	Tc=	=1.0 min CN=98	Runoff=1.64 cfs 4,856 cf
Reach 1R: Long Island Sound			Inflow=3.00 cfs 7,844 cf
5			Outflow=3.00 cfs 7,844 cf
Pond 1P: Rain Garden	Peak Elev=12.74	4' Storage=418 c	f Inflow=1.64 cfs 4,856 cf
Discarded=0	.51 cfs 4,384 cf Primary=	=0.82 cfs 472 cf	Outflow=1.33 cfs 4,856 cf
Pond 2P: 20 Linear Feet 1.0-Foot Diame	eter HDPE Peak Elev=10	0.41' Storage=21	cf Inflow=0.82 cfs 472 cf
		-	Outflow=0.84 cfs 472 cf
Total Pupoff Area = 40.54	9 cf Bunoff Volume = 1	12 228 of Avor	ao Bunoff Donth - 2 62"

Total Runoff Area = 40,549 sf Runoff Volume = 12,228 cfAverage Runoff Depth = 3.62"67.93% Pervious = 27,544 sf32.07% Impervious = 13,005 sf

Summary for Subcatchment 1: Watershed 1

Runoff = 2.30 cfs @ 12.10 hrs, Volume= 7,372 cf, Depth= 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.12"

	A	rea (sf)	CN	Description					
*		994	98	Existing rea	Existing rear walls, walk, steps				
*		78	98	Spa & wall					
		27,544	80	>75% Gras	- 75% Grass cover, Good, HSG D				
		28,616	81	Weighted Average					
		27,544		96.25% Pervious Area					
		1,072		3.75% Impervious Area					
(1	Tc min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description			
	6.9	92	0.0370	0.22		Sheet Flow, A->DP-1 Grass: Short n= 0.150	P2= 3.45"		

Summary for Subcatchment 1A: Watershed 1A

Runoff = 1.64 cfs @ 12.01 hrs, Volume= 4,856 cf, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 10-Year Rainfall=5.12"

	Area (sf)	CN	Description		
*	2,464	98	Pool & Poo	l deck	
*	5,322	98	Proposed F	Residence	
*	980	98	Proposed T	errace	
*	3,167	98	Proposed D	Driveway	
	11,933	98	Weighted A	verage	
	11,933		100.00% In	npervious A	rea
T (miı	c Length n) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description
1.	.0				Direct Entry, Direct Entry

Summary for Reach 1R: Long Island Sound

Inflow Are	a =	40,549 sf,	32.07% Impervious,	Inflow Depth = 2.32"	for 10-Year event
Inflow	=	3.00 cfs @	12.09 hrs, Volume=	7,844 cf	
Outflow	=	3.00 cfs @	12.09 hrs, Volume=	7,844 cf, Atte	n= 0%, Lag= 0.0 min
Summary for Pond 1P: Rain Garden

Inflow Are	a =	11,933 sf,10	0.00% Impervious,	Inflow Depth = 4.	88" for 10-Year event
Inflow	= 1	.64 cfs @ 1	2.01 hrs, Volume=	4,856 cf	
Outflow	= 1	.33 cfs @ 12	2.05 hrs, Volume=	4,856 cf,	Atten= 19%, Lag= 2.2 min
Discarded	= 0	.51 cfs @ 1	2.05 hrs, Volume=	4,384 cf	·
Primary	= 0	.82 cfs @ 12	2.05 hrs, Volume=	472 cf	
Routing by	y Stor-Ind r	nethod, Time	Span= 0.00-60.00	hrs, dt= 0.01 hrs / 3	
Peak Elev	= 12.74' @) 12.05 hrs S	Surf.Area= 728 sf	Storage= 418 cf	
Plug-Flow	detention	time= 2.8 min	calculated for 4,85	5 cf (100% of inflow	/)
Center-of-	Mass det.	time= 2.9 mir	n(745.8 - 743.0)		
	المتعرب المراجع	As sold Other			
volume	Invert	Avail.Sto	rage Storage Des	cription	
#1	12.00'	6	18 cf Custom Stag	ge Data (Prismatic)	Listed below (Recalc)
- 1	0			0	
Elevation	SL	Irr.Area	Inc.Store	Cum.Store	
(Teet)		(sq-ft)	(cubic-teet) (<u>cubic-teet)</u>	
12.00		394	0	0	
13.00		842	618	618	
Device F	Routing	Invert	Outlet Devices		
#1 [Discarded	12.00'	30.000 in/hr Exfilt	tration over Surfac	e area
#1 [#2 F	Discarded Primary	12.00' 12.50'	8.0" Horiz. Orifice	e/ Grate C= 0.600	e area Limited to weir flow at low heads

Discarded OutFlow Max=0.51 cfs @ 12.05 hrs HW=12.74' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.51 cfs)

Primary OutFlow Max=0.83 cfs @ 12.05 hrs HW=12.74' (Free Discharge) **2=Orifice/Grate** (Weir Controls 0.83 cfs @ 1.62 fps)

ry for Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE [Solid] 2.5-Inch Orifice @ 9.0 FT, 8.0-Inch Orifice @

Inflow Area	a =	11,933 sf,	,100.00% In	npervious,	Inflow Depth =	0.47"	for 10-Year event
Inflow	=	0.82 cfs @	12.05 hrs,	Volume=	472 c	f	
Outflow	=	0.84 cfs @	12.05 hrs,	Volume=	472 c	f, Atter	n= 0%, Lag= 0.0 min
Primary	=	0.84 cfs @	12.05 hrs,	Volume=	472 c	f	-

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 10.41' @ 12.05 hrs Surf.Area= 4 sf Storage= 21 cf

Plug-Flow detention time= 0.9 min calculated for 472 cf (100% of inflow) Center-of-Mass det. time= 0.8 min (726.8 - 725.9)

Volume	Invert	Avail.Storage	Storage Description
#1	9.00'	16 cf	12.0" Round Pipe Storage
			L= 20.0'
#2	9.00'	10 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		26 cf	Total Available Storage

Type III 24-hr 10-Year Rainfall=5.12" Printed 4/2/2019 Page 13

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Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
9.0	00	4	0	0				
11.5	50	4	10	10				
Device	Routing	Invert	Outlet Devices					
#1	Primary	9.00'	2.5" Vert. Orific	e/Grate C=	0.600			
#2	Primary	9.92'	8.0" Vert. Orific	e/Grate C=	0.600			
Primary	rimary OutFlow Max=0.84 cfs @ 12.05 hrs HW=10.41' (Free Discharge)							

-1=Orifice/Grate (Orifice Controls 0.19 cfs @ 5.50 fps) -2=Orifice/Grate (Orifice Controls 0.65 cfs @ 2.38 fps)

Proposed Condition - 2019-03-27		Type III 24-hr 25-Year Rainfall=6.41"
Prepared by Hudson Engineering & Col	nsulting, P.C.	Printed 4/2/2019
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Time span=0.00 Runoff by SCS TI Reach routing by Stor-Ind+T)-60.00 hrs, dt=0.01 hrs R-20 method, UH=SCS Trans method - Pond r	s, 6001 points 5, Weighted-CN routing by Stor-Ind method
Subcatchment 1: Watershed 1 Flow Length=92'	Runoff Area=28,616 Slope=0.0370 '/' Tc=6	sf 3.75% Impervious Runoff Depth=4.26" 6.9 min CN=81 Runoff=3.15 cfs 10,157 cf
Subcatchment 1A: Watershed 1A	Runoff Area=11,933 sf Tc=	100.00% Impervious Runoff Depth=6.17" =1.0 min CN=98 Runoff=2.05 cfs 6,137 cf
Reach 1R: Long Island Sound		Inflow=4.13 cfs 11,010 cf Outflow=4.13 cfs 11,010 cf
Pond 1P: Rain Garden Discarded=0.54	Peak Elev=12.87 4 cfs 5,284 cf Primary=	7' Storage=510 cf Inflow=2.05 cfs 6,137 cf =1.02 cfs 853 cf Outflow=1.56 cfs 6,137 cf
Pond 2P: 20 Linear Feet 1.0-Foot Diamete	r HDPE Peak Elev=10	0.51' Storage=22 cf Inflow=1.02 cfs 853 cf Outflow=1.04 cfs 853 cf
Total Runoff Area = 40,549	sf Runoff Volume = 1 67.93% Pervious = 27,	I6,294 cf Average Runoff Depth = 4.82" ,544 sf 32.07% Impervious = 13,005 sf

Summary for Subcatchment 1: Watershed 1

Runoff = 3.15 cfs @ 12.10 hrs, Volume= 10,157 cf, Depth= 4.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	Area	(sf)	CN	Description						
*	9	994	98	Existing rea	ar walls, wa	lk, steps				
*		78	98	Spa & wall						
	27,	544	80	>75% Gras	s cover, Go	ood, HSG D				
	28,	616	81	Weighted A	Weighted Average					
	27,	544		96.25% Pe	96.25% Pervious Area					
	1,	072		3.75% Impe	3.75% Impervious Area					
(m	Tc Le nin) (ngth feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description				
	6.9	92	0.037	0 0.22		Sheet Flow, A->DP-1 Grass: Short n= 0.150	P2= 3.45"			

Summary for Subcatchment 1A: Watershed 1A

Runoff = 2.05 cfs @ 12.01 hrs, Volume= 6,137 cf, Depth= 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 25-Year Rainfall=6.41"

	Area (sf)	CN	Description					
*	2,464	98	Pool & Poo	l deck				
*	5,322	98	Proposed F	Residence				
*	980	98	Proposed T	errace				
*	3,167	98	Proposed D	Proposed Driveway				
	11,933	98	Weighted Average					
	11,933		100.00% Impervious Area					
T (min	c Length	Slop	e Velocity	Capacity	Description			
		(101		(015)				
1.	0				Direct Entry, Direct Entry			

Summary for Reach 1R: Long Island Sound

Inflow Area	a =	40,549 sf,	32.07% Impervious,	Inflow Depth = 3.26"	for 25-Year event
Inflow	=	4.13 cfs @	12.09 hrs, Volume=	11,010 cf	
Outflow	=	4.13 cfs @	12.09 hrs, Volume=	11,010 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

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Summary for Pond 1P: Rain Garden

Inflow Are	ea = =	11,933 sf,10 2.05 cfs @ 1	0.00% Impervious 2.01 hrs. Volume	s, Inflow Depth = 6. = 6.137 cf	17" for 25-Year event
Outflow	=	1.56 cfs @ 1	2.06 hrs. Volume	= 6.137 cf.	Atten= 24%. Lag= 2.7 min
Discarde	d =	0.54 cfs @ 1	2.06 hrs, Volume	= 5,284 cf	, 3
Primary	=	1.02 cfs 🥘 1	2.06 hrs, Volume	= 853 cf	
Routing b	by Stor-Ind	method, Time	Span= 0.00-60.00) hrs, dt= 0.01 hrs / 3	
Peak Ele	v= 12.87' (2) 12.06 hrs S	Surf.Area= 783 sf	Storage= 510 cf	
	v dotontion	timo-20 min	a coloulated for 6.1	26 of (1000/ of inflow	0
Contor of	n detention f Mass det	time= 2.9 mir	$(742.4 \ 730.5)$		()
Center-0	I-INIASS UCL	. ume= 2.9 mi	1 (742.4 - 739.5)		
Volume	Inver	t Avail.Sto	rage Storage De	scription	
#1	12.00	' 6 [·]	18 cf Custom St	age Data (Prismatic)	Listed below (Recalc)
	0	C A			
Elevation	n S	urf.Area	Inc.Store	Cum.Store	
(feet	[)	(sq-π)		(cubic-teet)	
12.0	0	394	0	0	
13.0	0	842	618	618	
Davias	Douting	Invort	Outlat Daviaga		
Device	Routing	Invert	Outlet Devices		
#1	Discarded	12.00'	30.000 in/hr Exf	Itration over Surfac	e area
#2	Primary	12.50'	8.0" Horiz. Orific	ce/Grate C= 0.600	Limited to weir flow at low heads

Discarded OutFlow Max=0.54 cfs @ 12.06 hrs HW=12.87' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.54 cfs)

Primary OutFlow Max=1.02 cfs @ 12.06 hrs HW=12.87' (Free Discharge) **2=Orifice/Grate** (Orifice Controls 1.02 cfs @ 2.92 fps)

ry for Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE [Solid] 2.5-Inch Orifice @ 9.0 FT, 8.0-Inch Orifice @

Inflow Area	a =	11,933 sf,	,100.00% In	npervious,	Inflow Depth =	0.86"	for 25-Year event
Inflow	=	1.02 cfs @	12.06 hrs,	Volume=	853 c	f	
Outflow	=	1.04 cfs @	12.05 hrs,	Volume=	853 c	f, Atter	n= 0%, Lag= 0.0 min
Primary	=	1.04 cfs @	12.05 hrs,	Volume=	853 c	f	-

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 10.51' @ 12.05 hrs Surf.Area= 4 sf Storage= 22 cf

Plug-Flow detention time= 0.7 min calculated for 853 cf (100% of inflow) Center-of-Mass det. time= 0.7 min (726.7 - 726.1)

Volume	Invert	Avail.Storage	Storage Description
#1	9.00'	16 cf	12.0" Round Pipe Storage
			L= 20.0'
#2	9.00'	10 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		26 cf	Total Available Storage

Type III 24-hr 25-Year Rainfall=6.41" Printed 4/2/2019 Page 17

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Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
9.0	00	4	0	0	
11.5	50	4	10	10	
Device	Routing	Invert	Outlet Devices		
#1	Primary	9.00'	2.5" Vert. Orifice	e/Grate C=	0.600
#2	Primary	9.92'	8.0" Vert. Orifice	e/Grate C=	0.600
Primary	OutFlow	Max=1.04 cfs (@ 12.05 hrs HW=	10.50' (Fre	e Discharge)

-1=Orifice/Grate (Orifice Controls 0.19 cfs @ 5.70 fps) -2=Orifice/Grate (Orifice Controls 0.84 cfs @ 2.60 fps)

Proposed Condition - 2019-03-27		Type III 24-hr	50-Year Rainfall=7.60"
Prepared by Hudson Engineering & Cor	nsulting, P.C.		Printed 4/2/2019
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Time span=0.00	0-60.00 hrs, dt=0.01 hrs,	6001 points	nd method
Runoff by SCS TF	R-20 method, UH=SCS,	Weighted-CN	
Reach routing by Stor-Ind+T	Trans method - Pond ro	uting by Stor-Ir	
Subcatchment 1: Watershed 1	Runoff Area=28,616 s	f 3.75% Imper	vious Runoff Depth=5.37"
Flow Length=92'	Slope=0.0370 '/' Tc=6.9	9 min CN=81	Runoff=3.94 cfs 12,796 cf
Subcatchment 1A: Watershed 1A	Runoff Area=11,933 sf	100.00% Imper	vious Runoff Depth=7.36"
	Tc=1	.0 min CN=98	Runoff=2.44 cfs 7,319 cf
Reach 1R: Long Island Sound		(Inflow=5.08 cfs 14,024 cf Outflow=5.08 cfs 14,024 cf
Pond 1P: Rain Garden	Peak Elev=12.99'	Storage=608 c	f Inflow=2.44 cfs 7,319 cf
Discarded=0.58 d	cfs 6,091 cf Primary=1.1	7 cfs 1,228 cf	Outflow=1.75 cfs 7,319 cf
Pond 2P: 20 Linear Feet 1.0-Foot Diamete	r Peak Elev=10.59	' Storage=22 c	f Inflow=1.17 cfs 1,228 cf Outflow=1.18 cfs 1,228 cf
Total Runoff Area = 40,549 s	sf Runoff Volume = 20	,115 cf Avera	age Runoff Depth = 5.95"
	67.93% Pervious = 27,5	44 sf 32.07%	⁄⁄6 Impervious = 13,005 sf

Summary for Subcatchment 1: Watershed 1

Runoff = 3.94 cfs @ 12.10 hrs, Volume= 12,796 cf, Depth= 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=7.60"

	Are	ea (sf)	CN	Description					
*		994	98	Existing rea	ar walls, wa	lk, steps			
*		78	98	Spa & wall					
	2	7,544	80	>75% Gras	s cover, Go	ood, HSG D			
	2	8,616	81	Weighted A	verage				
	2	7,544		96.25% Pervious Area					
		1,072		3.75% Impervious Area					
(m	Tc l nin)	Length (feet)	Slop (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description			
	6.9	92	0.037	0.22		Sheet Flow, A->DP-1 Grass: Short n= 0.150	P2= 3.45"		

Summary for Subcatchment 1A: Watershed 1A

Runoff = 2.44 cfs @ 12.01 hrs, Volume= 7,319 cf, Depth= 7.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 50-Year Rainfall=7.60"

	Area (sf)	CN	Description		
*	2,464	98	Pool & Poo	l deck	
*	5,322	98	Proposed F	Residence	
*	980	98	Proposed T	errace	
*	3,167	98	Proposed D	Driveway	
	11,933	98	Weighted A	verage	
	11,933		100.00% In	npervious A	rea
T (mir	c Length) (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description
1.	0				Direct Entry, Direct Entry

Summary for Reach 1R: Long Island Sound

Inflow Area	a =	40,549 sf,	32.07% Impervious,	Inflow Depth = 4.15"	for 50-Year event
Inflow	=	5.08 cfs @	12.09 hrs, Volume=	14,024 cf	
Outflow	=	5.08 cfs @	12.09 hrs, Volume=	14,024 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

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Summary for Pond 1P: Rain Garden

Inflow Area	a =	11,933 sf	f,100.00%	Impervic	ous, Inflow Depth = 7.36" for 50-Year event			
Inflow	=	2.44 cfs @	12.01 hr	s, [`] Volum	ne= 7,319 cf			
Outflow	=	1.75 cfs @	12.07 hr	s, Volum	ne= 7,319 cf, Atten= 28%, Lag= 3.1 min			
Discarded	=	0.58 cfs @	12.07 hr	s, Volum	ne= 6,091 cf			
Primary	=	1.17 cfs @	12.07 hr	s, Volum	ne= 1,228 cf			
Routing by Peak Elev=	Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 12.99' @ 12.07 hrs Surf.Area= 836 sf Storage= 608 cf							
Plug-Flow detention time= 2.9 min calculated for 7,318 cf (100% of inflow) Center-of-Mass det. time= 2.9 min (740.2 - 737.2)								
Volume	Invei	t Avail.S	Storage	Storage I	Description			
#1	12.00)'	618 cf	Custom	Stage Data (Prismatic) Listed below (Recalc)			
Elevation	S	Surf.Area	Inc.	Store	Cum.Store			

tion	Surt.Area	Inc.Store	Cum.Store
eet)	(sq-ft)	(cubic-feet)	(cubic-feet)
2.00	394	0	0
3.00	842	618	618

Device	Routing	Invert	Outlet Devices		
#1	Discarded	12.00'	30.000 in/hr Exfiltration o	ver Surface	e area
#2	Primary	12.50'	8.0" Horiz. Orifice/Grate	C= 0.600	Limited to weir flow at low heads

Discarded OutFlow Max=0.58 cfs @ 12.07 hrs HW=12.99' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.58 cfs)

Primary OutFlow Max=1.17 cfs @ 12.07 hrs HW=12.99' (Free Discharge) **2=Orifice/Grate** (Orifice Controls 1.17 cfs @ 3.36 fps)

ry for Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE [Solid] 2.5-Inch Orifice @ 9.0 FT, 8.0-Inch Orifice @

Inflow Area	a =	11,933 sf,	100.00% Imp	pervious,	Inflow Depth =	1.24"	for 50-Year	event
Inflow	=	1.17 cfs @	12.07 hrs, \	/olume=	1,228 (cf		
Outflow	=	1.18 cfs @	12.06 hrs, \	/olume=	1,228 0	cf, Atter	n= 0%, Lag= 0).0 min
Primary	=	1.18 cfs @	12.06 hrs, \	/olume=	1,228 0	cf	-	

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 10.59' @ 12.06 hrs Surf.Area= 4 sf Storage= 22 cf

Plug-Flow detention time= 0.6 min calculated for 1,228 cf (100% of inflow) Center-of-Mass det. time= 0.6 min (726.8 - 726.2)

Volume	Invert	Avail.Storage	Storage Description
#1	9.00'	16 cf	12.0" Round Pipe Storage
			L= 20.0'
#2	9.00'	10 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		26 cf	Total Available Storage

Type III 24-hr 50-Year Rainfall=7.60" Printed 4/2/2019 Page 21

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Elevatio (fee	on et)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
9.0	00	4	0	0	
11.5	50	4	10	10	
Device	Routing	Invert	Outlet Devices		
#1	Primary	9.00'	2.5" Vert. Orific	e/Grate C=	0.600
#2	Primary	9.92'	8.0" Vert. Orific	e/Grate C=	0.600
Primary	OutFlow	Max=1.17 cfs (@ 12.06 hrs HW=	=10.59' (Fre	e Discharge)

-1=Orifice/Grate (Orifice Controls 0.20 cfs @ 5.86 fps) -2=Orifice/Grate (Orifice Controls 0.97 cfs @ 2.78 fps)

Water Quality Calculations



Proposed Condition - 2019-03-27	Type III 24-hr 1-WQv Rainfall=1.66"
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HydroCAD® 10.00-14 s/n 02549 © 2015 HydroCAD Softw	vare Solutions LLC Page 2
Time span=0.00-60.00 hrs, Runoff by SCS TR-20 metho	dt=0.01 hrs, 6001 points d, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans metho	d - Pond routing by Stor-Ind method
Subcatchment 1: Watershed 1 Runoff A Flow Length=92' Slope=0	Area=28,616 sf 3.75% Impervious Runoff Depth=0.40" 0.0370 '/' Tc=6.9 min CN=81 Runoff=0.26 cfs 956 cf
Subcatchment 1A: Watershed 1A Runoff Are	a=11,933 sf 100.00% Impervious Runoff Depth=1.44" Tc=1.0 min CN=98 Runoff=0.51 cfs 1,430 cf
Reach 1R: Long Island Sound	Inflow=0.26 cfs 956 cf Outflow=0.26 cfs 956 cf
Pond 1P: Rain GardenPeaDiscarded=0.32 cfs1,43	ak Elev=12.15' Storage=63 cf Inflow=0.51 cfs 1,430 cf 30 cf Primary=0.00 cfs 0 cf Outflow=0.32 cfs 1,430 cf
Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE	Peak Elev=9.00' Storage=0 cf Inflow=0.00 cfs 0 cf Outflow=0.00 cfs 0 cf
Total Runoff Area = 40,549 sf Runof 67.93% Per	f Volume = 2,386 cf Average Runoff Depth = 0.71" vious = 27,544 sf 32.07% Impervious = 13,005 sf

Summary for Subcatchment 1: Watershed 1

Runoff = 0.26 cfs @ 12.11 hrs, Volume= 956 cf, Depth= 0.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-WQv Rainfall=1.66"

	A	rea (sf)	CN	Description					
*		994	98	Existing rea	r walls, wa	lk, steps			
*		78	98	Spa & wall		-			
		27,544	80	>75% Gras	s cover, Go	ood, HSG D			
		28,616	81	Weighted A	verage				
		27,544		96.25% Pervious Area					
		1,072		3.75% Impervious Area					
(n	Tc nin)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description			
	6.9	92	0.0370	0.22		Sheet Flow, A->DP-1 Grass: Short n= 0.150	P2= 3.45"		

Summary for Subcatchment 1A: Watershed 1A

Runoff = 0.51 cfs @ 12.01 hrs, Volume= 1,430 cf, Depth= 1.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Type III 24-hr 1-WQv Rainfall=1.66"

	Area (sf)	CN	Description			
*	2,464	98	Pool & Poo	l deck		
*	5,322	98	Proposed F	Residence		
*	980	98	Proposed T	errace		
*	3,167	98	Proposed D	Driveway		
	11,933	98	Weighted A			
	11,933		100.00% In	npervious A	rea	
T (min	c Length	Slop	e Velocity	Capacity	Description	
		(101		(015)		
1.	0				Direct Entry, Direct Entry	

Summary for Reach 1R: Long Island Sound

Inflow Are	a =	40,549 sf,	32.07% Impervious	s, Inflow Depth = 0	.28" for 1-WQv event
Inflow	=	0.26 cfs @	12.11 hrs, Volume	= 956 cf	
Outflow	=	0.26 cfs @	12.11 hrs, Volume	= 956 cf,	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs

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Summary for Pond 1P: Rain Garden

Inflow Area =		11,933 sf,10	0.00% Impervious	Inflow Depth = 1	.44" for 1-WQv event	
Inflow	=	0.51 cfs @ 12	2.01 hrs, Volume=	1,430 cf		
Outflow	=	0.32 cfs @ 12	2.08 hrs, Volume=	1,430 cf,	Atten= 37%, Lag= 4.0 min	
Discardeo	= t	0.32 cfs @ 12	2.08 hrs, Volume=	1,430 cf		
Primary	=	0.00 cfs @ 0	0.00 hrs, Volume=	0 cf		
Routing b	y Stor-Ind	method, Time	Span= 0.00-60.00	hrs, dt= 0.01 hrs / 3	3	
Peak Elev	/= 12.15' (@ 12.08 hrs S	ourf.Area= 460 sf	Storage= 63 cf		
Dlug Elow	<i>d</i> atantiar	timo-08 min	colculated for 1.42	0 of (100% of inflow		
Center_of	Mass dot	time = 0.6 min	$(768 \ 1 - 767 \ 8)$		v)	
Center-or		. une- 0.0 mm	(700.4 - 707.0)			
Volume	Inver	t Avail.Stor	age Storage Des	scription		
#1	12.00)' 61	8 cf Custom Sta	ge Data (Prismatic) Listed below (Recalc)	
				0 (,	
Elevatior	า 5	Surf.Area	Inc.Store	Cum.Store		
(feet))	(sq-ft)	(cubic-feet) (cubic-feet)		
12.00)	394	0	0		
13.00)	842	618	618		
Device	Routing	Invert	Outlet Devices			
#1	Discarded	l 12.00'	30.000 in/hr Exfil	tration over Surfac	e area	
#2	Primary	12.50'	8.0" Horiz. Orific	e/Grate C= 0.600	Limited to weir flow at low he	ads
Discarded OutFlow Max $= 0.32$ cfs @ 12.08 hrs HW $= 12.15^{\circ}$ (Free Discharge)						

Discarded OutFlow Max=0.32 cfs @ 12.08 hrs HW=12.15' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.32 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=12.00' (Free Discharge) ←2=Orifice/Grate (Controls 0.00 cfs)

ry for Pond 2P: 20 Linear Feet 1.0-Foot Diameter HDPE [Solid] 2.5-Inch Orifice @ 9.0 FT, 8.0-Inch Orifice @

Inflow Area	a =	11,933 sf,1	00.00% Impervious,	Inflow Depth = 0.00"	for 1-WQv event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0 cf, Atter	n= 0%, Lag= 0.0 min
Primary	=	0.00 cfs @	0.00 hrs, Volume=	0 cf	-

Routing by Stor-Ind method, Time Span= 0.00-60.00 hrs, dt= 0.01 hrs Peak Elev= 9.00' @ 0.00 hrs Surf.Area= 4 sf Storage= 0 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	9.00'	16 cf	12.0" Round Pipe Storage
			L= 20.0'
#2	9.00'	10 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
		26 cf	Total Available Storage

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Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
9.00		4 0		0		
11.50		4 10		10		
Device Routing #1 Primary #2 Primary		Invert 9.00' 9.92'	Outlet Devices 2.5" Vert. Orifice 8.0" Vert. Orifice	e/ Grate C= e/ Grate C=	0.600 0.600	
Primary 1=Or 2=Or	Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=9.00' (Free Discharge) 1=Orifice/Grate (Controls 0.00 cfs) 2=Orifice/Grate (Controls 0.00 cfs)					

Deep Hole Test Logs

		1		Hereite			
SOIL	TESTING,	, INC.	TEST PITS CLIENT: STOPHEN WANG ASSOCI				
90 I OXF	ONOVAN	RD. 6478	PROJECT NO. 6-46 - 0647 - 17 TEST PIT NO: TP-1 2 4 3				
CT	(203) 262-9 (914) 946-4	328 850	PROJECT NAME # 7 PAIR AUGE				
	(0.1) 0.10 1		LOCATION				
BACKHOE OF	PD AT)	LARCAMONET, NY.				
INSPECTOR:			·		DATE WORK DONE:		
					3-15-17		
Test Pit	Water Level		Soil Strata in	Auger Holes	Remarks: Include: Groundwater depth, Size of		
or Probe No.	/ time elapsed	Moisture	From (ft.)	To (ft.)	Auger used, description of soil in Auger holes, depth of auger samples		
TP-1	Nione	Mair		GH	- mcni.		
	OHRS	martit	[] [] []	2'9'1	The The safe is the inthe led		
		1710101		20	RAID DEC LITTLE SAND, JEARCH		
		<u> </u>			BUUDUCOS (POSSIBLE FILL)		
		MOIST	3'8"	4'6"	PACTIALLY DECOMPOSED BEDROCK		
				4'6"	REFUSAL - GND of PIT		
					TNU PETCOLATION TEST PERFORMED DUE TO		
				High Brojock Conditions			
TP-2	None	maist	0	8 ^{<i>n</i>}	Topsail intre sano		
	OHRS			8"	BeDrock - Refusit - End of Pit		
				+ NO COLLAN			
TP-3	None	moist	0	1'6=	Topsoic Little SAND, GRAVEL		
	Ottres			1'G#	BEDrock - Refusing on of pit		
					¥ No		